

Company Name -

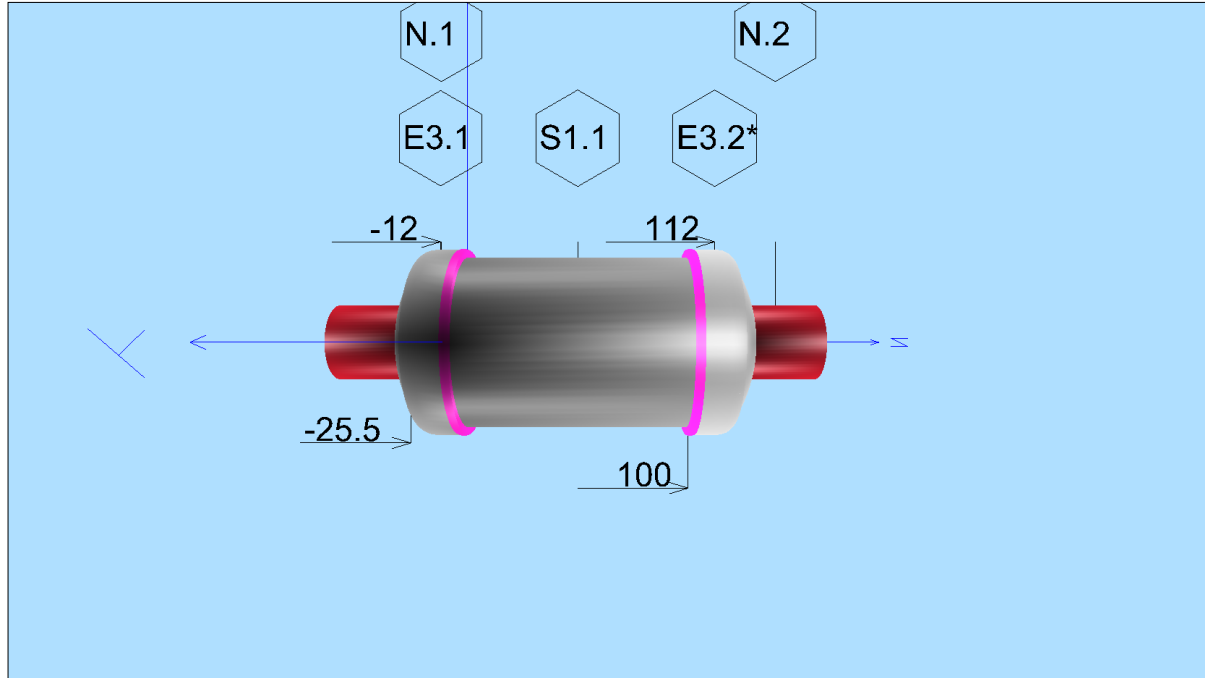
Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

(0) Drawing

3D View of Vessel (alter by using the Save User Specified View command)



Design Data & Process Information

Description	Units	Design Data
Process Card		General Design Data
Design Code & Specifications		EN13445 TG = 3b
Internal Design Pressure (MPa)	MPa	4.5
External Design Pressure (MPa)	MPa	
Hydrotest Pressure (MPa)	MPa	
Maximum Design Temperature (°C)	°C	130
Minimum Design Temperature (°C)	°C	-20
Operating Temperature (°C)	°C	
Corrosion Allowance (mm)	mm	0.5
Content of Vessel		
Specific Density of Oper.Liq		
Normal Liquid Level NLL (mm)	mm	

Utilization Chart

Utilization Chart

Company Name -

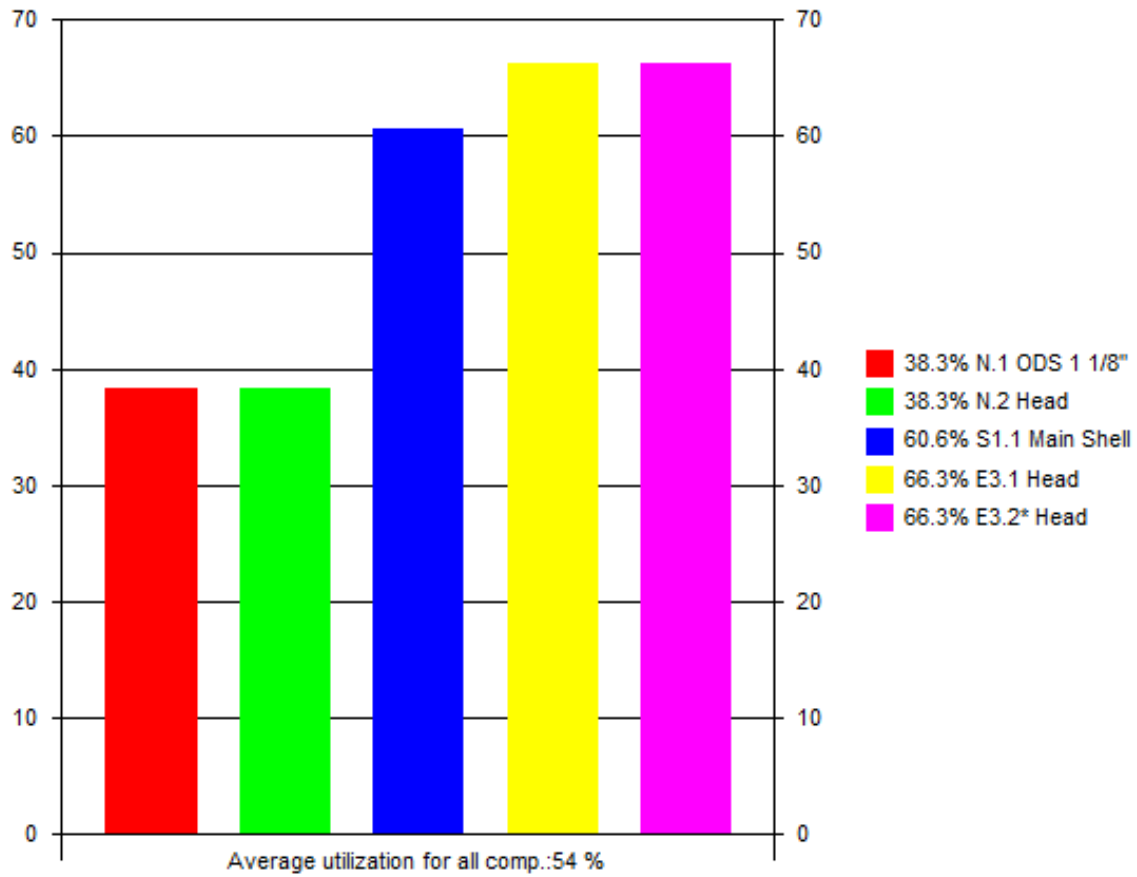
Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator :

Rev.:A

COMPONENTS UTILIZATION CHART - Client :GÜVEN SOGUTMA Vessel Tag No.:MF.45B.28.



Maximum Utilization of 66.3% for Component E3.1 Head - VVD by Hexagon PPM, Ver:20.0

Welding Information

EN1708-1 Welding Requirements for Pressurized Components

NOTE: No welding information has been specified by the user.

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.4.2 CYLINDRICAL SHELL

S1.1 Main Shell 31 May 2023 17:44

INPUT DATA

COMPONENT ATTACHMENT/LOCATION

Distance from end of cylinder to ref. DATUM LINE....:mm 0.00 mm

GENERAL DESIGN DATA

PRESSURE LOADING: Design Component for Internal Pressure Only

PROCESS CARD:

General Design Data : Temp= 130°C, P=4.5000 MPa, c=0.5 mm, Pext=0.0000 MPa

SPECIFIC DENSITY OF OPERATING LIQUID.....:SG 0.00

LIQUID HEAD.....:LH 0.00 mm

SHELL DATA

CYLINDER FABRICATION: Welded Pipe

WELD JOINT COEFFICIENT: Testing Group 3 (z=0.85)

NEGATIVE TOLERANCE: Negative tolerance specified in mm

EN 10217-3:2019, 1.0565 P355NH welded tube, HT:N THK<=20mm 130'C

Rm=490 Rp=355 Rpt=292 f=194.67 f20=204.17 ftest=338.1 E=203868(N/mm²) ro=7.85

OUTSIDE DIAMETER OF SHELL.....:De 76.00 mm

LENGTH OF CYLINDRICAL PART OF SHELL.....:Lcyl 100.00 mm

NOMINAL WALL THICKNESS (uncorroded).....:en 3.0000 mm

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....:th 0.3000 mm

Split shell into several shell courses and include welding information: NO

WELDING REQUIREMENTS TO EN 1708-1:2010

Comment(Optional):

Type of welded connection: Not Applicable

CALCULATION DATA

7.4.2 - CYLINDRICAL SHELLS UNDER INTERNAL PRESSURE

Required Minimum Shell Thickness Excl.Allow. emin :

$$emin = De * P / (2 * f * z + P) \quad (7.4-2)$$
$$= 76 * 4.5 / (2 * 194.67 * 0.85 + 4.5) = 1.0196 \text{ mm}$$

Required Minimum Shell Thickness Incl.Allow. :

$$emina = emin + c + NegDev = 1.02 + 0.5 + 0.3 = 1.8196 \text{ mm}$$

Analysis Thickness

$$ea = en - c - NegDev = 3 - 0.5 - 0.3 = 2.2000 \text{ mm}$$

»7.4.1 Cond.of Applicability $emin/De=0.0134 \leq 0.16$ » OK«

Internal Pressure $emina=1.82 \leq en=3$ [mm]	60.6%	OK
---	-------	----

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :

Inside Diameter of Shell

$$Di = De - 2 * ea = 76 - 2 * 2.2 = 71.60 \text{ mm}$$

Mean Diameter of Shell

$$Dm = (De + Di) / 2 = (76 + 71.6) / 2 = 73.80 \text{ mm}$$

MAWP HOT & CORR. (Corroded condition at design temp.)

$$MAWPHC = 2 * f * z * ea / Dm = 2 * 194.67 * 0.85 * 2.2 / 73.8 = 9.8654 \text{ MPa}$$

MAWP NEW & COLD (Uncorroded condition at ambient temp.)

$$MAWPNC = 2 * f20 * z * (ea + c) / Dm$$
$$= 2 * 204.17 * 0.85 * (2.2 + 0.5) / 73.8 = 12.70 \text{ MPa}$$

MAX TEST PRESSURE (Uncorroded cond.at ambient temp.)

Ptmax = 2 * ftest * ztest * (ea + c) / Dm

$$= 2 * 338.1 * 1 * (2.2 + 0.5) / 73.8 = 24.74 \text{ MPa}$$

Company Name -

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Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.4.2 CYLINDRICAL SHELL

S1.1 Main Shell 31 May 2023 17:44

EN13445-5;10.2.3.3 REQUIRED MIN.HYDROSTATIC TEST PRESSURE:Ptmin

NEW AT AMBIENT TEMP. FOR TEST GROUPS 1, 2 and 3

$$Ptmin = 1.25 * Pd * f_{20} / f = 1.25 * 4.5 * 204.17 / 194.67 = 5.8995 \text{ MPa}$$

$$Ptmin = 1.43 * Pd = 1.43 * 4.5 = 6.4350 \text{ MPa}$$

Test Pressure Ptmin=6.435 <= Pmax=24.74[MPa]	26.0%	OK
--	--------------	-----------

MAXIMUM DIAMETER OF UNREINFORCED OPENING IN SHELL

Inside Radius of Shell

$$ris = Di / 2 (9.5-3) = 71.6 / 2 = 35.80 \text{ mm}$$

Length of Shell Contributing to Reinforcement

$$Is = Sqr((2 * ris + ea) * ea) (9.5-2) = Sqr((2 * 35.8 + 2.2) * 2.2) = 12.74 \text{ mm}$$

Maximum Diameter of Unreinforced Opening in Shell Checked to Rules in Section 9

$$dmax1 = MIN(0.5 * Di, (ea * Is * (f - 0.5 * P) / P - ris * Is) / (0.5 * ris + 0.5 * ea)) (9.5-7, 22, 23) \\ = MIN(0.5 * 71.6, (2.2 * 12.74 * (194.67 - 0.5 * 4.5) / 4.5 - 35.8 * 12.74) / (0.5 * 35.8 + 0.5 * 2.2)) = 35.80 \text{ mm}$$

Maximum diameter of Opening Not Requiring Reinforcement Check

$$dmax2 = 0.15 * Sqr((2 * ris + ea) * ea) (9.5-18) \\ = 0.15 * Sqr((2 * 35.8 + 2.2) * 2.2) = 1.9113 \text{ mm}$$

Maximum Diameter of Unreinforced Opening

$$dmax = MAX(dmax1, dmax2) = MAX(35.8, 1.91) = 35.80 \text{ mm}$$

CALCULATION SUMMARY**7.4.2 - CYLINDRICAL SHELLS UNDER INTERNAL PRESSURE**

Required Minimum Shell Thickness Excl.Allow. emin :

$$emin = De * P / (2 * f * z + P) (7.4-2) \\ = 76 * 4.5 / (2 * 194.67 * 0.85 + 4.5) = 1.0196 \text{ mm}$$

Required Minimum Shell Thickness Incl.Allow. :

$$emina = emin + c + NegDev = 1.02 + 0.5 + 0.3 = 1.8196 \text{ mm}$$

Internal Pressure emina=1.82 <= en=3[mm]	60.6%	OK
--	--------------	-----------

MAX TEST PRESSURE (Uncorroded cond.at ambient temp.)

Ptmax = 2 * ftest * ztest * (ea + c) / Dm

$$= 2 * 338.1 * 1 * (2.2 + 0.5) / 73.8 = 24.74 \text{ MPa}$$

EN13445-5;10.2.3.3 REQUIRED MIN.HYDROSTATIC TEST PRESSURE:Ptmin

NEW AT AMBIENT TEMP. FOR TEST GROUPS 1, 2 and 3

$$Ptmin = 1.25 * Pd * f_{20} / f = 1.25 * 4.5 * 204.17 / 194.67 = 5.8995 \text{ MPa}$$

$$Ptmin = 1.43 * Pd = 1.43 * 4.5 = 6.4350 \text{ MPa}$$

Test Pressure Ptmin=6.435 <= Pmax=24.74[MPa]	26.0%	OK
--	--------------	-----------

MAXIMUM DIAMETER OF UNREINFORCED OPENING IN SHELL

Maximum Diameter of Unreinforced Opening

$$dmax = MAX(dmax1, dmax2) = MAX(35.8, 1.91) = 35.80 \text{ mm}$$

Volume:0.0004026 m3 Weight:0.5 kg (SG= 7.85)

Company Name -

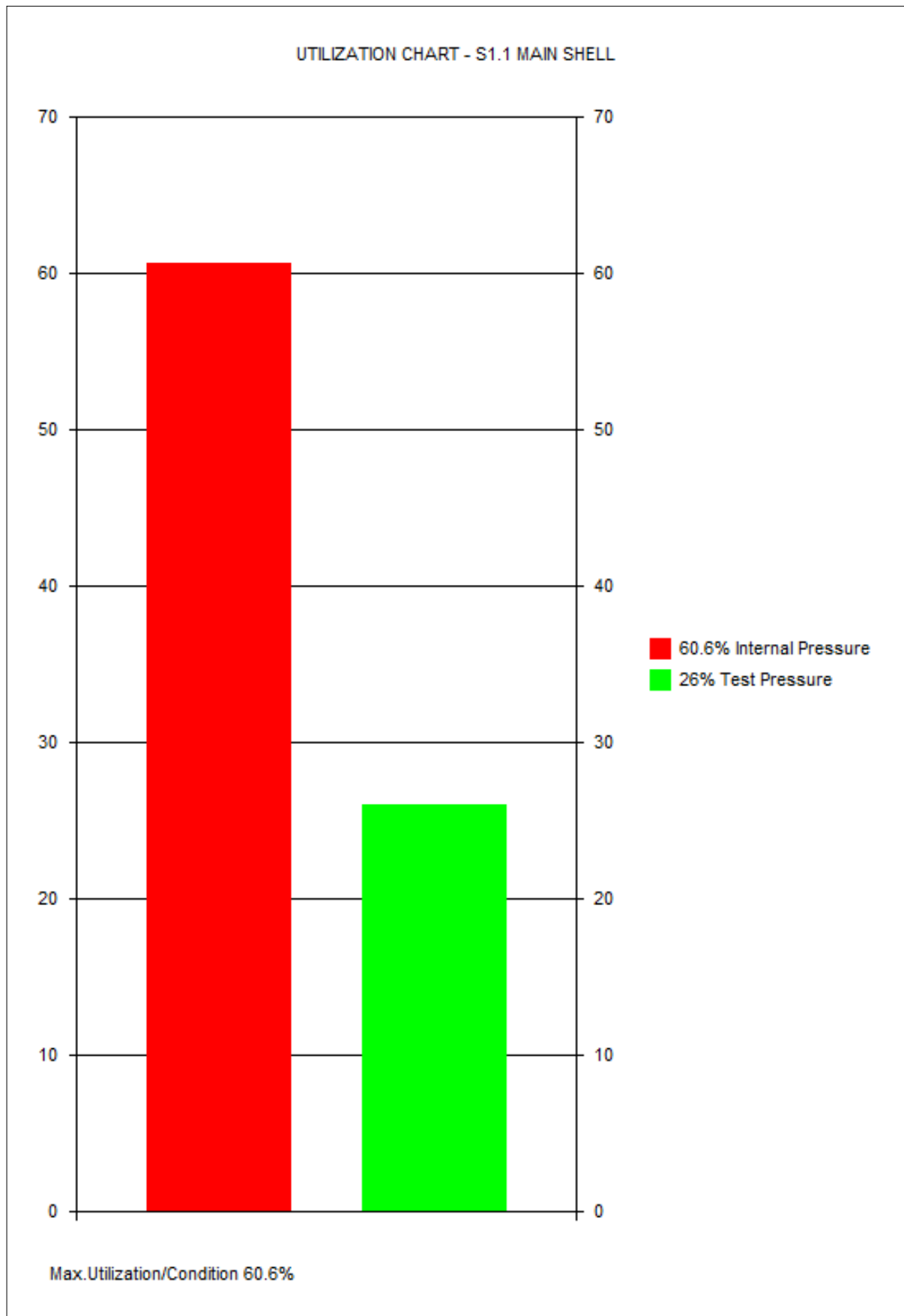
Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.4.2 CYLINDRICAL SHELL

S1.1 Main Shell 31 May 2023 17:44



Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Head 31 May 2023 17:48 ConnID:S1.1

INPUT DATA

COMPONENT ATTACHMENT/LOCATION

Attachment: S1.1 Cylindrical Shell Main Shell
Location: Along z-axis zo= 0

GENERAL DESIGN DATA

PRESSURE LOADING: Design Component for Internal Pressure Only

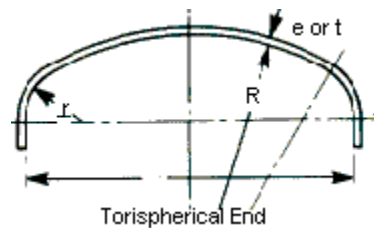
PROCESS CARD:

General Design Data : Temp= 130°C, P=4.5000 MPa, c=0.5 mm, Pext=0.0000 MPa

SPECIFIC DENSITY OF OPERATING LIQUID.....:SG 0.00

LIQUID HEAD.....:LH 38.80 mm

DIMENSIONS OF END



Type of Torispherical End: Dished End NOT listed above

WELD JOINT COEFFICIENT: Testing Group 3 (z=0.85)

OUTSIDE DIAMETER OF CYLINDRICAL FLANGE OF END.....:De 82.60 mm

LENGTH OF CYLINDRICAL FLANGE OF END.....:Lcyl 12.00 mm

INSIDE SPHERICAL RADIUS (corroded).....:R 63.00 mm

DEPTH OF HEAD INCLUDING HEAD THICKNESS.....:h 15.00 mm

INSIDE KNUCKLE RADIUS (corroded).....:r 5.0000 mm

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....:th 0.3000 mm

NOMINAL THICKNESS OF HEAD/END (uncorroded).....:en 3.0000 mm

Include calculation of forming during fabrication to EN13445-4 Section 9.: NO

MATERIAL DATA FOR END

EN 10028-2:2017, 1.0473 P355GH plate and strip, HT:N THK<=16mm 130'C

Rm=510 Rp=355 Rpt=308.6 f=205.73 f20=212.5 ftest=338.1 E=203868(N/mm2) ro=7.85

Material & Delivery Form: NOT Cold Spun Seamless Austenitic Stainless Steel

NOZZLES IN KNUCKLE REGION TO SECTION 7.7

Nozzles In Knuckle Region: NO

WELDING REQUIREMENTS TO EN 1708-1:2010

Comment(Optional):

Type of welded connection: Not Applicable

CALCULATION DATA

7.5.3 - TORISPHERICAL ENDS UNDER INTERNAL PRESSURE

7.5.3.2 Required Minimum End Thickness

Required Thickness of End to Limit Membrane Stress in Central Part

$$e_s = P * R / (2 * f * z - 0.5 * P) \quad (7.5-1)$$

$$= 4.5 * 63 / (2 * 205.73 * 0.85 - 0.5 * 4.5) = 0.8158 \text{ mm}$$

$$f_b = R_{pt} / 1.5 \quad (7.5-4) = 308.6 / 1.5 = 205.73 \text{ N/mm}^2$$

Required Thickness of Knuckle to Avoid Plastic Buckling

$$e_b = (0.75 * R + 0.2 * D_i) * ((P / (111 * f_b)) * (D_i / r)^{0.825})^{(0.667)} \quad (7.5-3)$$

$$= (0.75 * 63 + 0.2 * 77.6) * ((4.5 / (111 * 205.73)) * (77.6 / 5)^{0.825})^{(0.667)} = 0.9584 \text{ mm}$$

7.5.3.5 Formulas for Calculation of Factor Beta

$$Y = \text{MIN}(e_{min} / R, 0.04) \quad (7.5-9) = \text{MIN}(1.18 / 63, 0.04) = 0.0188$$

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E3.1 Head 31 May 2023 17:48 ConnID:S1.1

$$Z = \text{LOG}(1 / Y) \text{ (7.5-10)} = \text{LOG}(1/0.0188) = 1.7264$$

$$X = r / Di \text{ (7.5-11)} = 5/80.23 = 0.0623$$

$$N = 1.006 - 1 / (6.2 + (90 * Y) ^ 4) \text{ (7.5-12)} = 1.006 - 1 / (6.2 + (90 * 0.0188) ^ 4) = 0.9363$$

$$\text{Beta006} = N * (-0.3635 * Z ^ 3 + 2.2124 * Z ^ 2 - 3.2937 * Z + 1.8873) \text{ (7.5-13)} = 0.9363 * (-0.3635 * 1.73 ^ 3 + 2.2124 * 1.73 ^ 2 - 3.2937 * 1.73 + 1.8873) = 0.8658$$

$$\text{Beta01} = N * (-0.1833 * Z ^ 3 + 1.0383 * Z ^ 2 - 1.2943 * Z + 0.837) \text{ (7.5-15)} = 0.9363 * (-0.1833 * 1.73 ^ 3 + 1.0383 * 1.73 ^ 2 - 1.2943 * 1.73 + 0.837) = 0.7060$$

$$\text{beta} = 25 * ((0.1 - X) * \text{Beta006} + (X - 0.06) * \text{Beta01}) \text{ (7.5-14)} = 25 * ((0.1 - 0.0623) * 0.8658 + (0.0623 - 0.06) * 0.706) = 0.8565$$

Required Thickness of Knuckle to Avoid Axisymmetric Yielding

$$e_y = \text{beta} * P * (0.75 * R + 0.2 * Di) / f \text{ (7.5-2)} = 0.8565 * 4.5 * (0.75 * 63 + 0.2 * 80.23) / 205.73 = 1.1859 \text{ mm}$$

NOTE 3, since $e_y(1.2) > 0.005 * Di(0.4)$ it is NOT necessary to calculate/consider e_b .

Required Minimum End Thickness Excl.Allow. e_{min} :

$$e_{min} = e_{min} = 1.19 = 1.1859 \text{ mm}$$

Required Minimum End Thickness Incl.Allow. :

$$e_{minA} = e_{min} + c + th = 1.19 + 0.5 + 0.3 = 1.9900 \text{ mm}$$

Internal Pressure $e_{minA}=1.99 \leq e_n=3$[mm]	66.3%	OK
--	--------------	-----------

Analysis Thickness

$$e_a = e_n - c - th = 3 - 0.5 - 0.3 = 2.2000 \text{ mm}$$

Inside Diameter of Shell

$$Di = De - 2 * (e_n - c) = 82.6 - 2 * (3 - 0.5) = 77.60 \text{ mm}$$

Mean Diameter of Shell

$$D_m = (De + Di) / 2 = (82.6 + 77.6) / 2 = 80.10 \text{ mm}$$

7.5.3.4 - Required Minimum Thickness of Straight Cylindrical Flange

$$L_{lim} = 0.2 * \text{SQRT}(Di * e_{min}) = 0.2 * \text{SQRT}(77.6 * 1.19) = 1.9186 \text{ mm}$$

Since $L_{cyl} > L_{lim}$, Required Thickness of Straight Cylindrical Flange to 7.4.2

Minimum Thickness of Straight Flange Excl. Allow.

$$e_{cyl} = P * Di / (2 * f * z - P) \text{ (7.4-1)} = 4.5 * 77.6 / (2 * 205.73 * 0.85 - 4.5) = 1.0115 \text{ mm}$$

Minimum Thickness of Straight Flange Incl.Corr. :

$$e_{cylA} = e_{cyl} + c = 1.01 + 0.5 = 1.5100 \text{ mm}$$

7.5.3.1 Conditions of Applicability - Torispherical Ends

- »Geometry Check $r=5 \leq 0.2 * Di$ [mm] « » OK«
- »Geometry Check $r=5 \geq 0.06 * Di=4.66$ [mm] « » OK«
- »Geometry Check $r=5 \geq 2 * e=2.37$ [mm] « » OK«
- »Geometry Check $e=1.19 \leq 0.08 * De=6.61$ [mm] « » OK«
- »Geometry Check $e_a=2.2 \geq 0.001 * De=0.0826$ [mm] « » OK«
- »Geometry Check $R=63 \leq De=82.6$ [mm] « » OK«

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :NEW & COLD

$$P_s = 2 * f * z * e_a / (R + 0.5 * e_a) \text{ (7.5-6)} = 2 * 212.5 * 0.85 * 2.7 / (62.5 + 0.5 * 2.7) = 15.28 \text{ MPa}$$

$$P_y = f * e_a / (\text{beta} * (0.75 * R + 0.2 * Di)) \text{ (7.5-7)} = 212.5 * 2.7 / (0.6072 * (0.75 * 62.5 + 0.2 * 77.6)) = 15.14 \text{ MPa}$$

$$P_b = 111 * f_b * (e_a / (0.75 * R + 0.2 * Di)) ^ 1.5 * (r / Di) ^ 0.825 \text{ (7.5-8)} = 111 * 236.67 * (2.7 / (0.75 * 62.5 + 0.2 * 77.6)) ^ 1.5 * (5 / 77.6) ^ 0.825 = 24.62 \text{ MPa}$$

$$P_{cyl} = 2 * e_a * f * z / (Di + e_a) = 2 * 2.7 * 212.5 * 0.85 / (77.6 + 2.7) = 12.15 \text{ MPa}$$

$$P_{max} \text{ (is the least of } P_s, P_y, P_b \text{ and } P_{cyl}) = P_{max} = 12.15 = 12.15 \text{ MPa}$$

$$P_{max} = 12.15 \text{ MPa}$$

$$P_{max} = 12.15 \text{ MPa}$$

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EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Head 31 May 2023 17:48 ConnID:S1.1

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :HOT & CORR

$$\begin{aligned}
 P_s &= 2 * f * z * e_a / (R + 0.5 * e_a) && (7.5-6) \\
 &= 2 * 205.73 * 0.85 * 2.2 / (63 + 0.5 * 2.2) = && 12.00 \text{ MPa} \\
 P_y &= f * e_a / (\beta * (0.75 * R + 0.2 * D_i)) && (7.5-7) \\
 &= 205.73 * 2.2 / (0.6502 * (0.75 * 63 + 0.2 * 77.6)) = && 11.09 \text{ MPa} \\
 P_B &= 111 * f_b * (e_a / (0.75 * R + 0.2 * D_i))^{1.5} * (r / D_i)^{0.825} && (7.5-8) \\
 &= 111 * 205.73 * (2.2 / (0.75 * 63 + 0.2 * 77.6))^{1.5} * (5 / 77.6)^{0.825} = && 15.60 \text{ MPa} \\
 P_{cyl} &= 2 * e_a * f * z / (D_i + e_a) \\
 &= 2 * 2.2 * 205.73 * 0.85 / (77.6 + 2.2) = && 9.6420 \text{ MPa} \\
 P_{max} & \text{ (is the least of } P_s, P_y, P_b \text{ and } P_{cyl}) = P_{max} \\
 &= 9.64 = && \underline{\underline{9.6420 \text{ MPa}}}
 \end{aligned}$$

MAX TEST PRESSURE (Uncorroded cond.at ambient temp.)

$$\begin{aligned}
 P_s &= 2 * f * z * e_a / (R + 0.5 * e_a) && (7.5-6) \\
 &= 2 * 338.1 * 1 * 2.7 / (62.5 + 0.5 * 2.7) = && 28.59 \text{ MPa} \\
 P_y &= f * e_a / (\beta * (0.75 * R + 0.2 * D_i)) && (7.5-7) \\
 &= 338.1 * 2.7 / (0.6072 * (0.75 * 62.5 + 0.2 * 77.6)) = && 24.09 \text{ MPa} \\
 P_B &= 111 * f_b * (e_a / (0.75 * R + 0.2 * D_i))^{1.5} * (r / D_i)^{0.825} && (7.5-8) \\
 &= 111 * 338.1 * (2.7 / (0.75 * 62.5 + 0.2 * 77.6))^{1.5} * (5 / 77.6)^{0.825} = && 35.17 \text{ MPa} \\
 P_{cyl} &= 2 * e_a * f * z / (D_i + e_a) \\
 &= 2 * 2.7 * 338.1 * 1 / (77.6 + 2.7) = && 22.74 \text{ MPa} \\
 P_{max} & \text{ (is the least of } P_s, P_y, P_b \text{ and } P_{cyl}) = P_{max} \\
 &= 22.74 = && \underline{\underline{22.74 \text{ MPa}}}
 \end{aligned}$$

EN13445-5;10.2.3.3 REQUIRED MIN.HYDROSTATIC TEST PRESSURE:Ptmin

NEW AT AMBIENT TEMP. FOR TEST GROUPS 1, 2 and 3

$$P_{tmin} = 1.25 * P_d * f_{20} / f = 1.25 * 4.5 * 212.5 / 205.73 = 5.8101 \text{ MPa}$$

$$P_{tmin} = 1.43 * P_d = 1.43 * 4.5 = 6.4350 \text{ MPa}$$

Test Pressure $P_{tmin} = 6.435 \leq P_{tmax} = 22.74$ [MPa]

28.3%

OK

Maximum diameter of Opening Not Requiring Reinforcement Check , dmax

$$\begin{aligned}
 r_{is} &= R \text{ (9.5-4)} = 63 = && 63.00 \text{ mm} \\
 \text{Length of Shell Contributing to Reinforcement} \\
 I_s &= \text{Sqr}((2 * r_{is} + e_a) * e_a) \text{ (9.5-2)} = \text{Sqr}((2 * 63 + 2.2) * 2.2) = && 16.79 \text{ mm} \\
 \text{Maximum Diameter of Unreinforced Opening in Shell Checked to Rules in Section 9} \\
 d_{max1} &= \text{MIN}(0.5 * D_i, (e_a * I_s * (f - 0.5 * P) / P - r_{is} * I_s) / (0.5 * r_{is} + 0.5 * e_a)) && (9.5-7, 22, 23) \\
 &= \text{MIN}(0.5 * 77.6, (2.2 * 16.79 * (205.73 - 0.5 * 4.5) / 4.5 - 63 * 16.79) / (0.5 * 63 + 0.5 * 2.2)) \\
 &= 18.79 \text{ mm} \\
 \text{Maximum diameter of Opening Not Requiring Reinforcement Check} \\
 d_{max2} &= 0.15 * \text{Sqr}((2 * r_{is} + e_a) * e_a) && (9.5-18) \\
 &= 0.15 * \text{Sqr}((2 * 63 + 2.2) * 2.2) = && 2.5191 \text{ mm} \\
 \text{Maximum Diameter of Unreinforced Opening} \\
 d_{max} &= \text{MAX}(d_{max1}, d_{max2}) = \text{MAX}(18.79, 2.52) = && \underline{\underline{18.79 \text{ mm}}}
 \end{aligned}$$

CALCULATION SUMMARY

7.5.3 - TORISPHERICAL ENDS UNDER INTERNAL PRESSURE

7.5.3.2 Required Minimum End Thickness

Required Minimum End Thickness Excl.Allow. e_{min} :

$$e_{min} = e_{min} = 1.19 = 1.1859 \text{ mm}$$

Required Minimum End Thickness Incl.Allow. :

$$e_{min_a} = e_{min} + c + t_h = 1.19 + 0.5 + 0.3 = 1.9900 \text{ mm}$$

Internal Pressure $e_{min_a} = 1.99 \leq e_n = 3$ [mm]

66.3%

OK

Minimum Thickness of Straight Flange Incl.Corr. :

$$e_{cyl_a} = e_{cyl} + c = 1.01 + 0.5 = 1.5100 \text{ mm}$$

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Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Head 31 May 2023 17:48 ConnID:S1.1

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :NEW & COLDPmax (is the least of Ps, Py, Pb and Pcyl) = Pmax
=12.15=12.15 MPa**MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :HOT & CORR**Pmax (is the least of Ps, Py, Pb and Pcyl) = Pmax
=9.64=9.6420 MPa**MAX TEST PRESSURE (Uncorroded cond.at ambient temp.)**Pmax (is the least of Ps, Py, Pb and Pcyl) = Pmax
=22.74=22.74 MPa**EN13445-5;10.2.3.3 REQUIRED MIN.HYDROSTATIC TEST PRESSURE:Ptmin**

NEW AT AMBIENT TEMP. FOR TEST GROUPS 1, 2 and 3

Ptmin = 1.25 * Pd * f20 / f =1.25*4.5*212.5/205.73=

5.8101 MPa

Ptmin = 1.43 * Pd =1.43*4.5=

6.4350 MPa**Test Pressure Ptmin=6.435 <= Pmax=22.74[MPa]****28.3%****OK****Maximum diameter of Opening Not Requiring Reinforcement Check , dmax**

Maximum Diameter of Unreinforced Opening

dmax = MAX(dmax1, dmax2) =MAX(18.79,2.52)=

18.79 mm

Volume:0.0000900 m3 Weight:0.2 kg (SG= 7.85)

Company Name -

Client :GÜVEN SOGUTMA

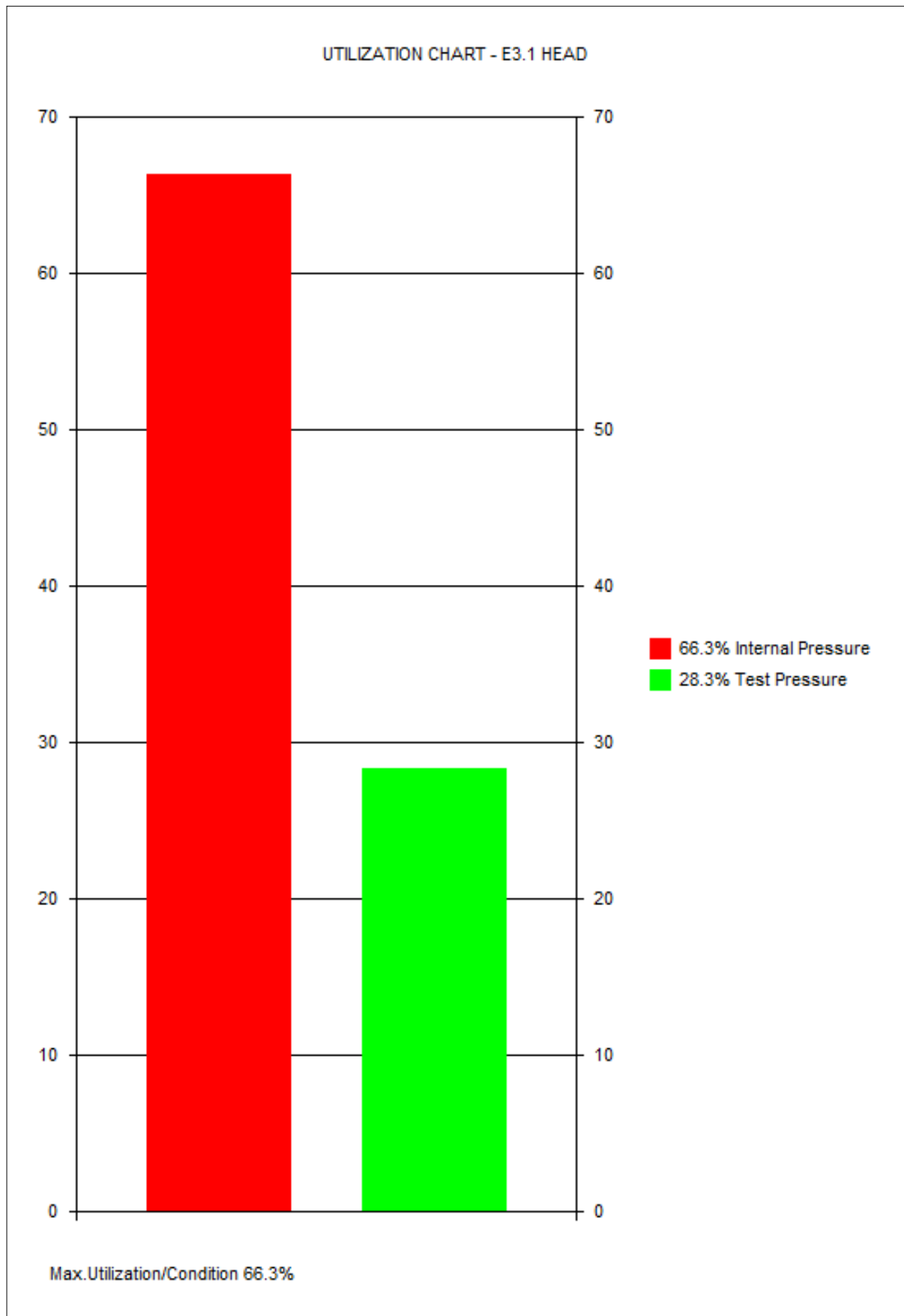
Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Head

31 May 2023 17:48 ConnID:S1.1



Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

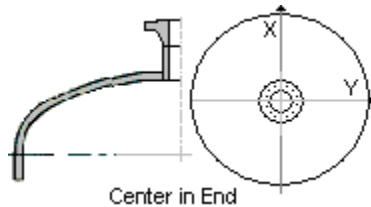
EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.1 ODS 1 1/8" 31 May 2023 17:51 ConnID:E3.1

INPUT DATA

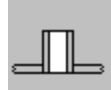
COMPONENT ATTACHMENT/LOCATION

Attachment: E3.1 Torispherical End Head S1.1
Connect this nozzle to the nozzle neck of another nozzle: NO



Orientation & Location of Nozzle: Center in End

GENERAL DESIGN DATA



Type of Opening: Nozzle Without Standard ASME or DIN/EN Flange Attachment
PRESSURE LOADING: Design Component for Internal Pressure Only

PROCESS CARD:

General Design Data : Temp= 130°C, P=4.5000 MPa, c=0.5 mm, Pext=0.0000 MPa

SPECIFIC DENSITY OF OPERATING LIQUID.....:SG 0.00

LIQUID HEAD.....:LH 0.00 mm

Apply a different corrosion allowance to nozzle neck than the shell thickness.: NO

Include Nozzle Load Calculation: NO

SHELL DATA (E3.1)

Shell Type: Torispherical End

OUTSIDE DIAMETER OF SHELL.....:De 82.60 mm

NOMINAL WALL THICKNESS (uncorroded).....:en 3.0000 mm

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....:th 0.3000 mm

INSIDE SPHERICAL RADIUS (corroded).....:R 63.00 mm

EN 10028-2:2017, 1.0473 P355GH plate and strip, HT:N THK<=16mm 130'C

Rm=510 Rp=355 Rpt=308.6 fs=205.73 f20=212.5 ftest=338.1 E=203868(N/mm2) ro=7.85

NOZZLE MATERIAL DATA



Delivery Form: Seamless Pipe

EN 10216-2:2013, 1.0345 P235GH seamless tube, HT:N THK<=16mm 130'C

Rm=360 Rp=235 Rpt=191.4 fb=127.6 f20=150 ftest=223.81 E=203868(N/mm2) ro=7.85

NOZZLE DIMENSIONAL DATA



Attachment: Set In Flush Nozzle

Shape of Nozzle/Opening: Circular

Application:

9.4.6.3 NOT a critical fatigue area, and calc.temp.is outside creep range.

OUTSIDE NOZZLE DIAMETER.....:deb 33.30 mm

NOMINAL NOZZLE THICKNESS (uncorroded).....:enb 5.1500 mm

Size of Flange and Nozzle:

Comment (Optional):

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....: 12.50 %

NOZZLE STANDOUT MEASURED FROM VESSEL OD.....:ho 30.00 mm

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

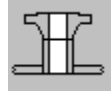
N.1 ODS 1 1/8"

31 May 2023 17:51 ConnID:E3.1

WELDING DATA

Nozzle/Pad to Shell Welding Area: Exclude Area of Nozzle to Shell Weld
Nozzle Weld Intersect: Nozzle Does NOT Intersect with a Welded Shell Seam
ANGLE BETWN.BRANCH AXIS AND A LINE NORMAL TO MAIN BODY:Phi 0.00 Degr.

DATA FOR REINFORCEMENT PAD



Type of Pad: No Pad

LIMITS OF REINFORCEMENT

Reduction of Limits of Reinforcement: No Reduction Required

WELDING REQUIREMENTS TO EN 1708-1:2010

Comment(Optional):

Type of welded connection: Not Applicable

CALCULATION DATA

PRELIMINARY CALCULATIONS

Shell Analysis Thickness eas 2.2000 mm
 $eas = en - c - th = 3 - 0.5 - 0.3 =$
Nozzle Analysis Thickness eab 4.0063 mm
 $eab = enb - cn - NegDev = 5.15 - 0.5 - 0.6438 =$
 $ris = R (9.5 - 4) = 63 =$ 63.00 mm
 $dib = deb - 2 * eab = 33.3 - 2 * 4.01 =$ 25.29 mm
Min.Nozzle Thk.Based on Internal Pressure ebp
 $ebp = P * deb / (2 * fb * z + P)$
 $= 4.5 * 33.3 / (2 * 127.6 * 1 + 4.5) =$ 0.5800 mm
Allowable Stresses
 $fob = Min(fs, fb) (9.5 - 8) = Min(205.73, 127.6) =$ 127.60 N/mm²

GEOMETRIC LIMITATIONS

»Check Max.Diameter of Nozzle $dib/De = 0.3061 \leq 0.60 = 0.6 [mm]$ (9.4.5.3)« OK«

Min.Nozzle Thk. $ebp = 0.58 \leq eab = 4.01 [mm]$	14.4%	OK
---	-------	----

»Location in End to Fig.9.5-4 $L = 24.65 \geq De/10 = 8.26 [mm]$ « » OK«

9.5.2.4.4 Nozzles normal to the shell, with or without reinforcement pads.

Calculation of Stress Loaded Areas Effective as Reinforcement

Area of Shell Afs

Limit of Reinforcement Along Shell Reduced by Location in Dished End
Iso = == 17.87 mm
Set In Nozzle
 $Afs = eas * Is (9.5-79) = 2.2 * 17.87 =$ 39.31 mm²

Area of Nozzle Afb

Limit of Reinforcement Along Nozzle (outside shell)
 $Ibo = MIN(Sqr((deb - eb) * eb), ho) (9.5-76)$
 $= MIN(Sqr((33.3 - 4.01) * 4.01), 30) =$ 10.83 mm
Set In Nozzle
 $Afb = eb * (Ibo + Ibi + eas) (9.5-78) = 4.01 * (10.83 + 0 + 2.2) =$ 52.21 mm²

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.1 ODS 1 1/8"

31 May 2023 17:51 ConnID:E3.1

Calculation of Pressure Loaded Areas

In the Nozzle Apb

$$Apb = 0.5 * dib * (Ibo + eas) \quad (9.5-84) = 0.5 * 25.29 * (10.83 + 2.2) = 164.79 \text{ mm}^2$$

Spherical Shell/End on any Section Aps

$$Aps = 0.5 * ris^2 * (Is + a) / (0.5 * eas + ris) \quad (9.5-105) \\ = 0.5 * 63^2 * (17.87 + 16.84) / (0.5 * 2.2 + 63) = 1074.66 \text{ mm}^2$$

9.5.2 Reinforcement Rules

Pressure Area Required pA(req.)

$$pAReq = P * (Aps + Apb + 0.5 * Apphi) \quad (9.5-7) \\ = 4.5 * (1074.66 + 164.79 + 0.5 * 0) = 5.5775 \text{ kN}$$

Pressure Area Available pA(aval.)

$$pAAval = (Afs + Afw) * (fs - 0.5 * P) + Afp * (fop - 0.5 * P) + Afb * (fob - 0.5 * P) \quad (9.5-7) \\ = (39.31 + 0) * (205.73 - 0.5 * 4.5) + 0 * (0 - 0.5 * 4.5) + 52.21 * (127.6 - 0.5 * 4.5) = 14.54 \text{ kN}$$

Nozzle Reinforcement pAAval=14.54 >= pAReq=5.58[kN]

38.3%

OK

Maximum Allowable Pressure Pmax

$$Pmax = (Afs + Afw) * fs + Afb * fob / ((Aps + Apb + 0.5 * Apphi) + 0.5 * (Afs + Afw + Afb + Afp)) \quad (9.5-10) \\ = (39.31 + 0) * 205.73 + 52.21 * 127.6 / ((1074.66 + 164.79 + 0.5 * 0) + 0.5 * (39.31 + 0 + 52.21 + 0)) \\ = 11.48 \text{ MPa}$$

Max.Allowable Test Pressure Pmax

$$Pmax = == 22.78 \text{ MPa}$$

Weight of Nozzle: .126kg

CALCULATION SUMMARY

Min.Nozzle Thk. ebp=0.58 <= eab=4.01[mm]

14.4%

OK

9.5.2.4 Nozzles normal to the shell, with or without reinforcement pads.

Limit of Reinforcement Along Shell Reduced by Location in Dished End

$$Iso = == 17.87 \text{ mm}$$

Limit of Reinforcement Along Nozzle (outside shell)

$$Ibo = \text{MIN}(\text{Sqr}((deb - eb) * eb), ho) \quad (9.5-76) \\ = \text{MIN}(\text{Sqr}((33.3 - 4.01) * 4.01), 30) = 10.83 \text{ mm}$$

Pressure Area Required pA(req.)

$$pAReq = P * (Aps + Apb + 0.5 * Apphi) \quad (9.5-7) \\ = 4.5 * (1074.66 + 164.79 + 0.5 * 0) = 5.5775 \text{ kN}$$

Pressure Area Available pA(aval.)

$$pAAval = (Afs + Afw) * (fs - 0.5 * P) + Afp * (fop - 0.5 * P) + Afb * (fob - 0.5 * P) \quad (9.5-7) \\ = (39.31 + 0) * (205.73 - 0.5 * 4.5) + 0 * (0 - 0.5 * 4.5) + 52.21 * (127.6 - 0.5 * 4.5) = 14.54 \text{ kN}$$

Nozzle Reinforcement pAAval=14.54 >= pAReq=5.58[kN]

38.3%

OK

Maximum Allowable Pressure Pmax

$$Pmax = (Afs + Afw) * fs + Afb * fob / ((Aps + Apb + 0.5 * Apphi) + 0.5 * (Afs + Afw + Afb + Afp)) \quad (9.5-10) \\ = (39.31 + 0) * 205.73 + 52.21 * 127.6 / ((1074.66 + 164.79 + 0.5 * 0) + 0.5 * (39.31 + 0 + 52.21 + 0)) \\ = 11.48 \text{ MPa}$$

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.1 ODS 1 1/8"

31 May 2023 17:51 ConnID:E3.1

Volume:0.00 m3 Weight:0.1 kg (SG= 7.85)

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.2 Head

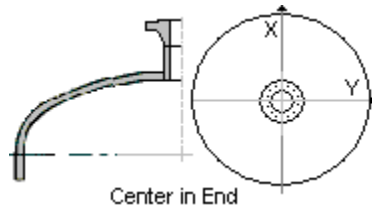
31 May 2023 17:52 ConnID:E3.2*

INPUT DATA

COMPONENT ATTACHMENT/LOCATION

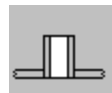
Attachment: E3.2* Torispherical End Head S1.1

Connect this nozzle to the nozzle neck of another nozzle: NO



Orientation & Location of Nozzle: Center in End

GENERAL DESIGN DATA



Type of Opening: Nozzle Without Standard ASME or DIN/EN Flange Attachment

PRESSURE LOADING: Design Component for Internal Pressure Only

PROCESS CARD:

General Design Data : Temp= 130°C, P=4.5000 MPa, c=0.5 mm, Pext=0.0000 MPa

SPECIFIC DENSITY OF OPERATING LIQUID.....:SG 0.00

LIQUID HEAD.....:LH 0.00 mm

Apply a different corrosion allowance to nozzle neck than the shell thickness.: NO

Include Nozzle Load Calculation: NO

SHELL DATA (E3.2*)

Shell Type: Torispherical End

OUTSIDE DIAMETER OF SHELL.....:De 82.60 mm

NOMINAL WALL THICKNESS (uncorroded).....:en 3.0000 mm

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....:th 0.3000 mm

INSIDE SPHERICAL RADIUS (corroded).....:R 63.00 mm

EN 10028-2:2017, 1.0473 P355GH plate and strip, HT:N THK<=16mm 130'C

Rm=510 Rp=355 Rpt=308.6 fs=205.73 f20=212.5 ftest=338.1 E=203868(N/mm2) ro=7.85

NOZZLE MATERIAL DATA

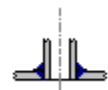


Delivery Form: Seamless Pipe

EN 10216-2:2013, 1.0345 P235GH seamless tube, HT:N THK<=16mm 130'C

Rm=360 Rp=235 Rpt=191.4 fb=127.6 f20=150 ftest=223.81 E=203868(N/mm2) ro=7.85

NOZZLE DIMENSIONAL DATA



Attachment: Set In Flush Nozzle

Shape of Nozzle/Opening: Circular

Application:

9.4.6.3 NOT a critical fatigue area, and calc.temp.is outside creep range.

OUTSIDE NOZZLE DIAMETER.....:deb 33.30 mm

NOMINAL NOZZLE THICKNESS (uncorroded).....:enb 5.1500 mm

Size of Flange and Nozzle:

Comment (Optional):

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....: 12.50 %

NOZZLE STANDOUT MEASURED FROM VESSEL OD.....:ho 30.00 mm

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.2 Head

31 May 2023 17:52 ConnID:E3.2*

WELDING DATA

Nozzle/Pad to Shell Welding Area: Exclude Area of Nozzle to Shell Weld
Nozzle Weld Intersect: Nozzle Does NOT Intersect with a Welded Shell Seam
ANGLE BETWN.BRANCH AXIS AND A LINE NORMAL TO MAIN BODY:Phi 0.00 Degr.

DATA FOR REINFORCEMENT PAD



Type of Pad: No Pad

LIMITS OF REINFORCEMENT

Reduction of Limits of Reinforcement: No Reduction Required

WELDING REQUIREMENTS TO EN 1708-1:2010

Comment(Optional):

Type of welded connection: Not Applicable

CALCULATION DATA

PRELIMINARY CALCULATIONS

Shell Analysis Thickness eas 2.2000 mm
 $eas = en - c - th = 3 - 0.5 - 0.3 =$
Nozzle Analysis Thickness eab 4.0063 mm
 $eab = enb - cn - NegDev = 5.15 - 0.5 - 0.6438 =$
 $ris = R (9.5 - 4) = 63 =$ 63.00 mm
 $dib = deb - 2 * eab = 33.3 - 2 * 4.01 =$ 25.29 mm
Min.Nozzle Thk.Based on Internal Pressure ebp
 $ebp = P * deb / (2 * fb * z + P)$
 $= 4.5 * 33.3 / (2 * 127.6 * 1 + 4.5) =$ 0.5800 mm
Allowable Stresses
 $fob = \text{Min}(fs, fb) (9.5 - 8) = \text{Min}(205.73, 127.6) =$ 127.60 N/mm²

GEOMETRIC LIMITATIONS

»Check Max.Diameter of Nozzle $dib/De = 0.3061 \leq 0.60 = 0.6[\text{mm}]$ (9.4.5.3)« OK«

Min.Nozzle Thk. $ebp = 0.58 \leq eab = 4.01[\text{mm}]$	14.4%	OK
---	-------	----

»Location in End to Fig.9.5-4 $L = 24.65 \geq De/10 = 8.26[\text{mm}]$ « » OK«

9.5.2.4.4 Nozzles normal to the shell, with or without reinforcement pads.

Calculation of Stress Loaded Areas Effective as Reinforcement

Area of Shell Afs

Limit of Reinforcement Along Shell Reduced by Location in Dished End
Iso = == 17.87 mm
Set In Nozzle
 $Afs = eas * Is (9.5-79) = 2.2 * 17.87 =$ 39.31 mm²

Area of Nozzle Afb

Limit of Reinforcement Along Nozzle (outside shell)
 $Ibo = \text{MIN}(\text{Sqr}((deb - eb) * eb), ho)$ (9.5-76)
 $= \text{MIN}(\text{Sqr}((33.3 - 4.01) * 4.01), 30) =$ 10.83 mm
Set In Nozzle
 $Afb = eb * (Ibo + Ibi + eas) (9.5-78) = 4.01 * (10.83 + 0 + 2.2) =$ 52.21 mm²

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.2 Head

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Calculation of Pressure Loaded Areas

In the Nozzle Apb

$$Apb = 0.5 * dib * (Ibo + eas) \quad (9.5-84) = 0.5 * 25.29 * (10.83 + 2.2) = 164.79 \text{ mm}^2$$

Spherical Shell/End on any Section Aps

$$Aps = 0.5 * ris^2 * (Is + a) / (0.5 * eas + ris) \quad (9.5-105) \\ = 0.5 * 63^2 * (17.87 + 16.84) / (0.5 * 2.2 + 63) = 1074.66 \text{ mm}^2$$

9.5.2 Reinforcement Rules

Pressure Area Required pA(req.)

$$pAReq = P * (Aps + Apb + 0.5 * Apphi) \quad (9.5-7) \\ = 4.5 * (1074.66 + 164.79 + 0.5 * 0) = 5.5775 \text{ kN}$$

Pressure Area Available pA(aval.)

$$pAAval = (Afs + Afw) * (fs - 0.5 * P) + Afp * (fop - 0.5 * P) + Afb * (fob - 0.5 * P) \quad (9.5-7) \\ = (39.31 + 0) * (205.73 - 0.5 * 4.5) + 0 * (0 - 0.5 * 4.5) + 52.21 * (127.6 - 0.5 * 4.5) = 14.54 \text{ kN}$$

Nozzle Reinforcement pAAval=14.54 >= pAReq=5.58[kN]

38.3%

OK

Maximum Allowable Pressure Pmax

$$Pmax = (Afs + Afw) * fs + Afb * fob / ((Aps + Apb + 0.5 * Apphi) + 0.5 * (Afs + Afw + Afb + Afp)) \quad (9.5-10) \\ = (39.31 + 0) * 205.73 + 52.21 * 127.6 / ((1074.66 + 164.79 + 0.5 * 0) + 0.5 * (39.31 + 0 + 52.21 + 0)) \\ = 11.48 \text{ MPa}$$

Max.Allowable Test Pressure Pmax

$$Pmax = == 22.78 \text{ MPa}$$

Weight of Nozzle: .126kg

CALCULATION SUMMARY

Min.Nozzle Thk. ebp=0.58 <= eab=4.01[mm]

14.4%

OK

9.5.2.4 Nozzles normal to the shell, with or without reinforcement pads.

Limit of Reinforcement Along Shell Reduced by Location in Dished End

$$Iso = == 17.87 \text{ mm}$$

Limit of Reinforcement Along Nozzle (outside shell)

$$Ibo = \text{MIN}(\text{Sqr}((deb - eb) * eb), ho) \quad (9.5-76) \\ = \text{MIN}(\text{Sqr}((33.3 - 4.01) * 4.01), 30) = 10.83 \text{ mm}$$

Pressure Area Required pA(req.)

$$pAReq = P * (Aps + Apb + 0.5 * Apphi) \quad (9.5-7) \\ = 4.5 * (1074.66 + 164.79 + 0.5 * 0) = 5.5775 \text{ kN}$$

Pressure Area Available pA(aval.)

$$pAAval = (Afs + Afw) * (fs - 0.5 * P) + Afp * (fop - 0.5 * P) + Afb * (fob - 0.5 * P) \quad (9.5-7) \\ = (39.31 + 0) * (205.73 - 0.5 * 4.5) + 0 * (0 - 0.5 * 4.5) + 52.21 * (127.6 - 0.5 * 4.5) = 14.54 \text{ kN}$$

Nozzle Reinforcement pAAval=14.54 >= pAReq=5.58[kN]

38.3%

OK

Maximum Allowable Pressure Pmax

$$Pmax = (Afs + Afw) * fs + Afb * fob / ((Aps + Apb + 0.5 * Apphi) + 0.5 * (Afs + Afw + Afb + Afp)) \quad (9.5-10) \\ = (39.31 + 0) * 205.73 + 52.21 * 127.6 / ((1074.66 + 164.79 + 0.5 * 0) + 0.5 * (39.31 + 0 + 52.21 + 0)) \\ = 11.48 \text{ MPa}$$

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.2 Head 31 May 2023 17:52 ConnID:E3.2*

Volume:0.00 m3 Weight:0.1 kg (SG= 7.85)

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:MF.45B.28.1

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.2 Head

31 May 2023 17:52 ConnID:E3.2*

