

Company Name -

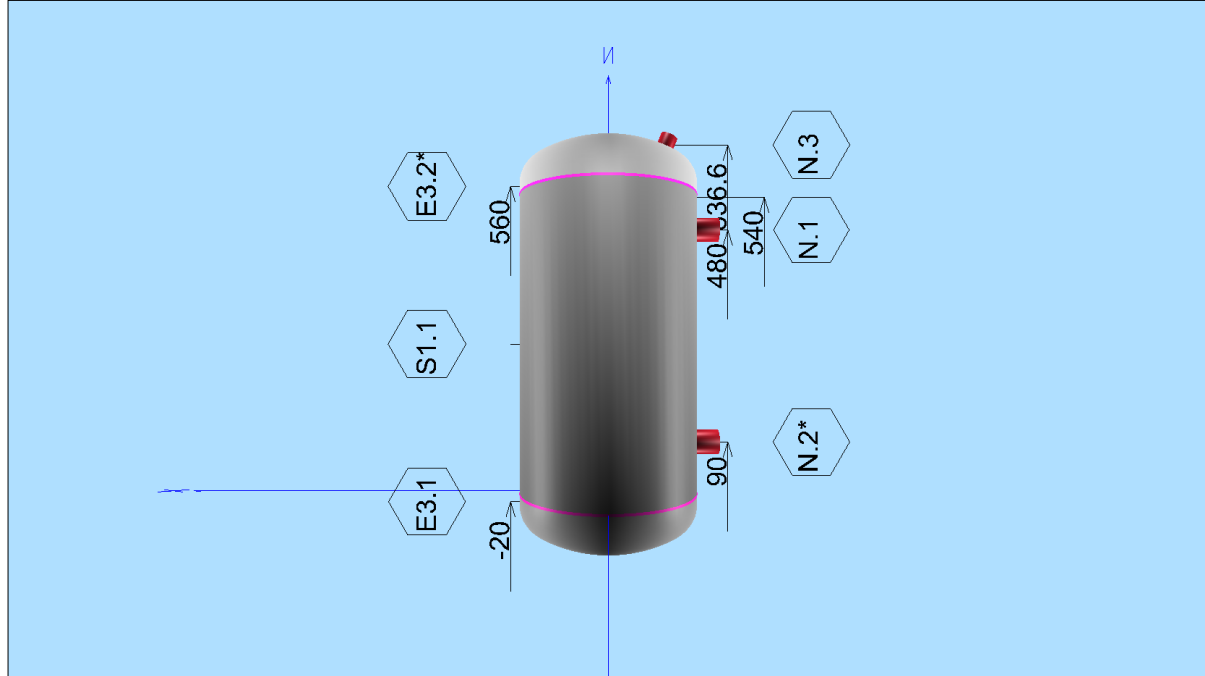
Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

(0) Drawing

3D View of Vessel (alter by using the Save User Specified View command)



Design Data & Process Information

Description	Units	Design Data
Process Card		General Design Data
Design Code & Specifications		EN13445 TG = 3b
Internal Design Pressure (MPa)	MPa	3.3
External Design Pressure (MPa)	MPa	
Hydrotest Pressure (MPa)	MPa	
Maximum Design Temperature (°C)	°C	130
Minimum Design Temperature (°C)	°C	-20
Operating Temperature (°C)	°C	
Corrosion Allowance (mm)	mm	0.5
Content of Vessel		
Specific Density of Oper.Liq		
Normal Liquid Level NLL (mm)	mm	

Utilization Chart

Utilization Chart

Company Name -

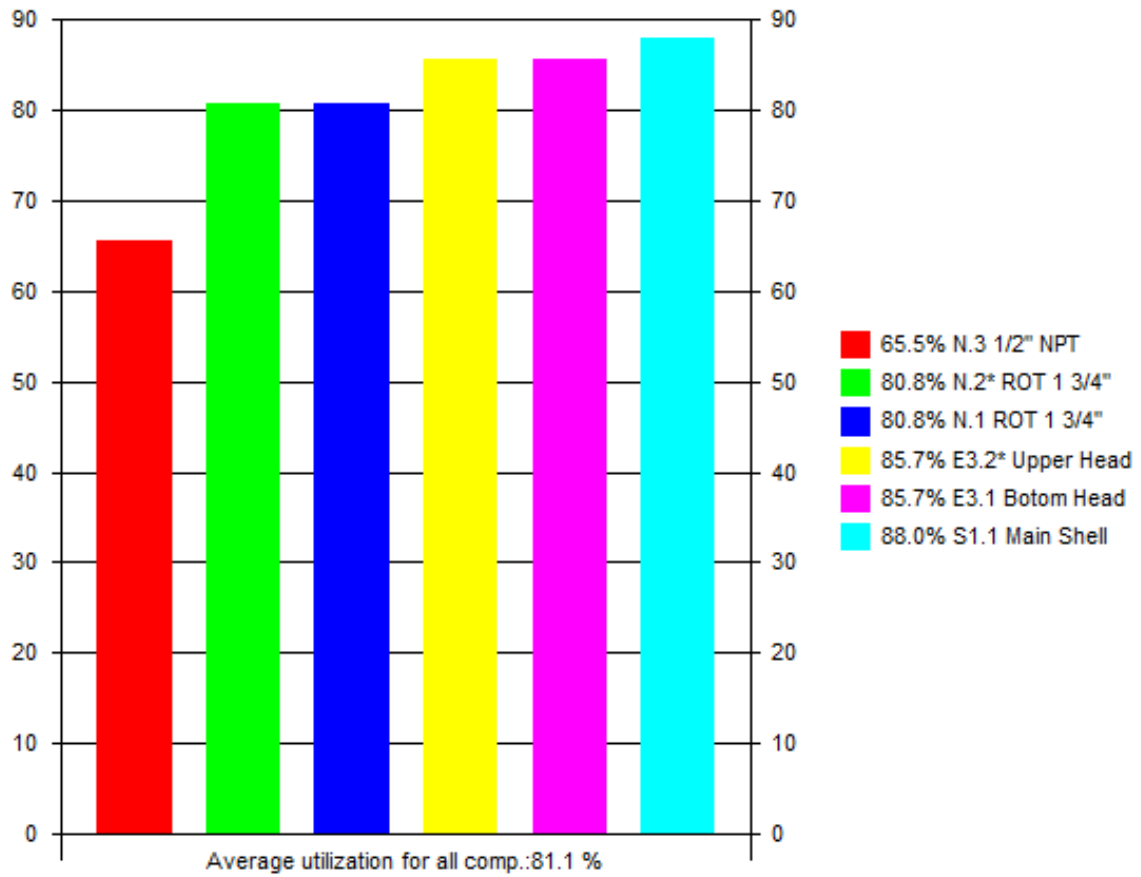
Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator :

Rev.:A

COMPONENTS UTILIZATION CHART - Client :GÜVEN SOGUTMA Vessel Tag No.:HV9.33b.60.A4.



Maximum Utilization of 88% for Component S1.1 Main Shell - VVD by Hexagon PPM, Ver:20.0

Welding Information

EN1708-1 Welding Requirements for Pressurized Components

NOTE: No welding information has been specified by the user.

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.4.2 CYLINDRICAL SHELL

S1.1 Main Shell 28 May 2023 11:40

INPUT DATA

COMPONENT ATTACHMENT/LOCATION

Distance from end of cylinder to ref. DATUM LINE....:mm 0.00 mm

GENERAL DESIGN DATA

PRESSURE LOADING: Design Component for Internal Pressure Only

PROCESS CARD:

General Design Data : Temp= 130°C, P=3.3000 MPa, c=0.5 mm, Pext=0.0000 MPa

SPECIFIC DENSITY OF OPERATING LIQUID.....:SG 0.00

LIQUID HEAD.....:LH 0.00 mm

SHELL DATA

CYLINDER FABRICATION: Welded Pipe

WELD JOINT COEFFICIENT: Testing Group 2 (z=1.0)

NEGATIVE TOLERANCE: Negative tolerance specified in mm

EN 10217-3:2019, 1.0565 P355NH welded tube, HT:N THK<=20mm 130'C

Rm=490 Rp=355 Rpt=292 f=194.67 f20=204.17 ftest=338.1 E=203868(N/mm2) ro=7.85

OUTSIDE DIAMETER OF SHELL.....:De 324.00 mm

LENGTH OF CYLINDRICAL PART OF SHELL.....:Lcyl 540.00 mm

NOMINAL WALL THICKNESS (uncorroded).....:en 4.0000 mm

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....:th 0.3000 mm

Split shell into several shell courses and include welding information: NO

WELDING REQUIREMENTS TO EN 1708-1:2010

Comment(Optional):

Type of welded connection: Not Applicable

CALCULATION DATA

7.4.2 - CYLINDRICAL SHELLS UNDER INTERNAL PRESSURE

Required Minimum Shell Thickness Excl.Allow. emin :

$$\text{emin} = \text{De} * \text{P} / (2 * \text{f} * \text{z} + \text{P}) \quad (7.4-2)$$
$$= 324 * 3.3 / (2 * 194.67 * 1 + 3.3) = 2.7231 \text{ mm}$$

Required Minimum Shell Thickness Incl.Allow. :

$$\text{emina} = \text{emin} + \text{c} + \text{NegDev} = 2.72 + 0.5 + 0.3 = 3.5231 \text{ mm}$$

Analysis Thickness

$$\text{ea} = \text{en} - \text{c} - \text{NegDev} = 4 - 0.5 - 0.3 = 3.2000 \text{ mm}$$

»7.4.1 Cond.of Applicability $\text{emin}/\text{De} = 0.0084 \leq 0.16$ » OK«

Internal Pressure $\text{emina} = 3.52 \leq \text{en} = 4$ [mm]

88.0%

OK

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :

Inside Diameter of Shell

$$\text{Di} = \text{De} - 2 * \text{ea} = 324 - 2 * 3.2 = 317.60 \text{ mm}$$

Mean Diameter of Shell

$$\text{Dm} = (\text{De} + \text{Di}) / 2 = (324 + 317.6) / 2 = 320.80 \text{ mm}$$

MAWP HOT & CORR. (Corroded condition at design temp.)

$$\text{MAWPHC} = 2 * \text{f} * \text{z} * \text{ea} / \text{Dm} = 2 * 194.67 * 1 * 3.2 / 320.8 = 3.8837 \text{ MPa}$$

MAWP NEW & COLD (Uncorroded condition at ambient temp.)

$$\text{MAWPNC} = 2 * \text{f20} * \text{z} * (\text{ea} + \text{c}) / \text{Dm}$$
$$= 2 * 204.17 * 1 * (3.2 + 0.5) / 320.8 = 4.7097 \text{ MPa}$$

MAX TEST PRESSURE (Uncorroded cond.at ambient temp.)

Ptmax = 2 * ftest * ztest * (ea + c) / Dm

$$= 2 * 338.1 * 1 * (3.2 + 0.5) / 320.8 = 7.7991 \text{ MPa}$$

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.4.2 CYLINDRICAL SHELL

S1.1 Main Shell 28 May 2023 11:40

EN13445-5;10.2.3.3 REQUIRED MIN.HYDROSTATIC TEST PRESSURE:Ptmin

NEW AT AMBIENT TEMP. FOR TEST GROUPS 1, 2 and 3

$$Ptmin = 1.25 * Pd * f_{20} / f = 1.25 * 3.3 * 204.17 / 194.67 = 4.3263 \text{ MPa}$$

$$Ptmin = 1.43 * Pd = 1.43 * 3.3 = 4.7190 \text{ MPa}$$

Test Pressure Ptmin=4.72 <= Pmax=7.8[MPa]	60.5%	OK
---	-------	----

MAXIMUM DIAMETER OF UNREINFORCED OPENING IN SHELL

Inside Radius of Shell

$$r_{is} = D_i / 2 \text{ (9.5-3)} = 317.6 / 2 = 158.80 \text{ mm}$$

Length of Shell Contributing to Reinforcement

$$I_s = \text{Sqr}((2 * r_{is} + e_a) * e_a) \text{ (9.5-2)}$$

$$= \text{Sqr}((2 * 158.8 + 3.2) * 3.2) = 32.04 \text{ mm}$$

Maximum Diameter of Unreinforced Opening in Shell Checked to Rules in Section 9

$$d_{max1} = \text{MIN}(0.5 * D_i, (e_a * I_s * (f - 0.5 * P) / (P - r_{is} * I_s)) / (0.5 * r_{is} + 0.5 * e_a)) \text{ (9.5-7,22,23)}$$

$$= \text{MIN}(0.5 * 317.6, (3.2 * 32.04 * (194.67 - 0.5 * 3.3) / (3.3 - 158.8 * 32.04)) / (0.5 * 158.8 + 0.5 * 3.2)) = 11.22 \text{ mm}$$

Maximum diameter of Opening Not Requiring Reinforcement Check

$$d_{max2} = 0.15 * \text{Sqr}((2 * r_{is} + e_a) * e_a) \text{ (9.5-18)}$$

$$= 0.15 * \text{Sqr}((2 * 158.8 + 3.2) * 3.2) = 4.8060 \text{ mm}$$

Maximum Diameter of Unreinforced Opening

$$d_{max} = \text{MAX}(d_{max1}, d_{max2}) = \text{MAX}(11.22, 4.81) = 11.22 \text{ mm}$$

CALCULATION SUMMARY**7.4.2 - CYLINDRICAL SHELLS UNDER INTERNAL PRESSURE**Required Minimum Shell Thickness Excl.Allow. e_{min} :

$$e_{min} = D_e * P / (2 * f * z + P) \text{ (7.4-2)}$$

$$= 324 * 3.3 / (2 * 194.67 * 1 + 3.3) = 2.7231 \text{ mm}$$

Required Minimum Shell Thickness Incl.Allow. :

$$e_{min_a} = e_{min} + c + \text{NegDev} = 2.72 + 0.5 + 0.3 = 3.5231 \text{ mm}$$

Internal Pressure $e_{min_a} = 3.52 \leq e_n = 4$ [mm]	88.0%	OK
--	-------	----

MAX TEST PRESSURE (Uncorroded cond.at ambient temp.)

$$P_{tmax} = 2 * f_{test} * z_{test} * (e_a + c) / D_m$$

$$= 2 * 338.1 * 1 * (3.2 + 0.5) / 320.8 = 7.7991 \text{ MPa}$$

EN13445-5;10.2.3.3 REQUIRED MIN.HYDROSTATIC TEST PRESSURE:Ptmin

NEW AT AMBIENT TEMP. FOR TEST GROUPS 1, 2 and 3

$$Ptmin = 1.25 * Pd * f_{20} / f = 1.25 * 3.3 * 204.17 / 194.67 = 4.3263 \text{ MPa}$$

$$Ptmin = 1.43 * Pd = 1.43 * 3.3 = 4.7190 \text{ MPa}$$

Test Pressure Ptmin=4.72 <= Pmax=7.8[MPa]	60.5%	OK
---	-------	----

MAXIMUM DIAMETER OF UNREINFORCED OPENING IN SHELL

Maximum Diameter of Unreinforced Opening

$$d_{max} = \text{MAX}(d_{max1}, d_{max2}) = \text{MAX}(11.22, 4.81) = 11.22 \text{ mm}$$

Volume:0.0428 m³ Weight:17 kg (SG= 7.85)

Company Name -

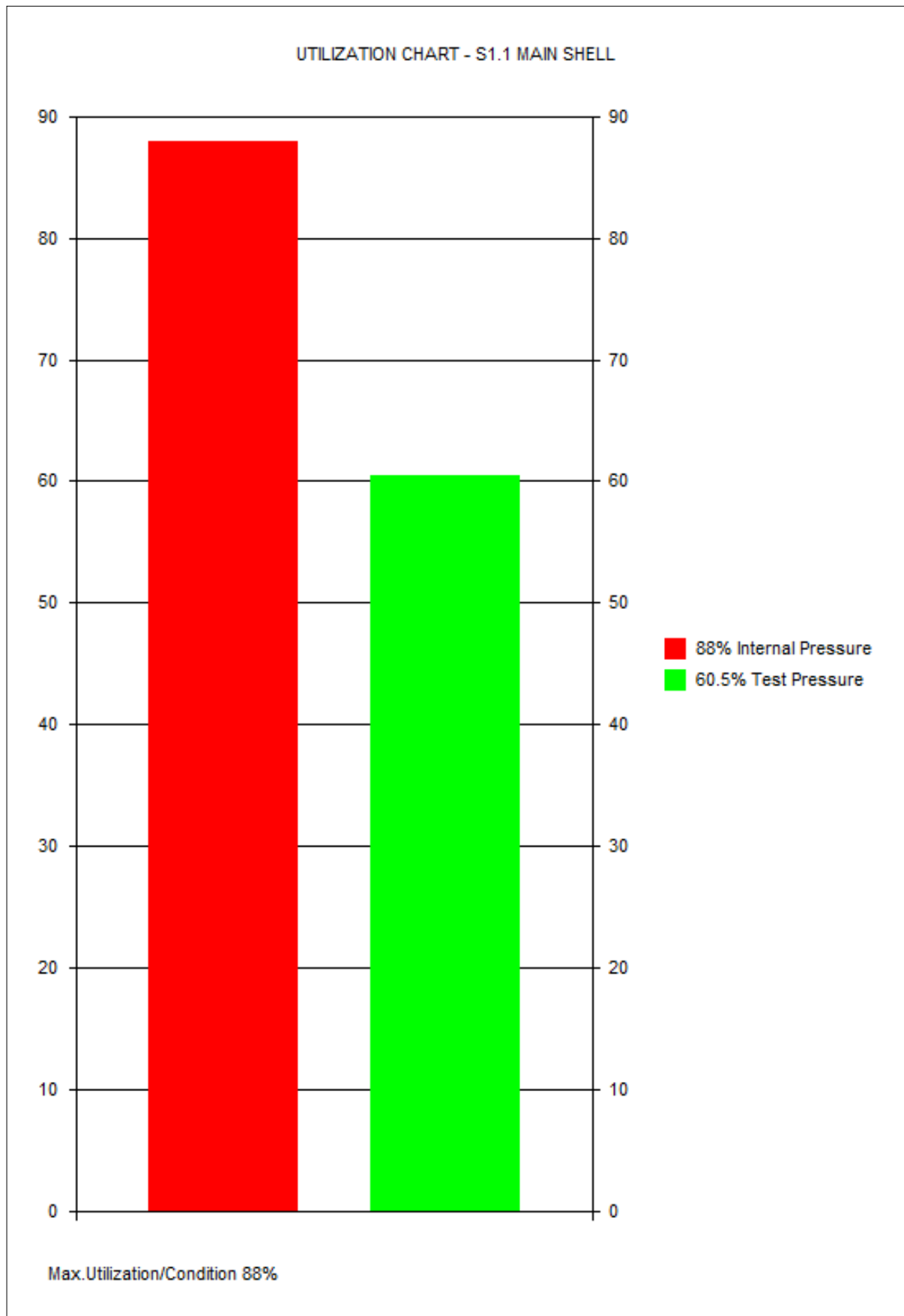
Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.4.2 CYLINDRICAL SHELL

S1.1 Main Shell 28 May 2023 11:40



Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Botom Head 28 May 2023 11:42 ConnID:S1.1

INPUT DATA

COMPONENT ATTACHMENT/LOCATION

Attachment: S1.1 Cylindrical Shell Main Shell
Location: Along z-axis zo= 0

GENERAL DESIGN DATA

PRESSURE LOADING: Design Component for Internal Pressure Only

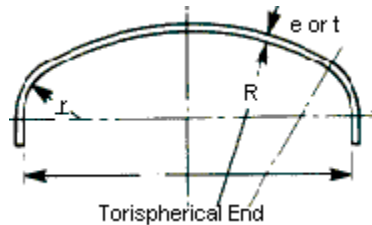
PROCESS CARD:

General Design Data : Temp= 130°C, P=3.3000 MPa, c=0.5 mm, Pext=0.0000 MPa

SPECIFIC DENSITY OF OPERATING LIQUID.....:SG 0.00

LIQUID HEAD.....:LH 0.00 mm

DIMENSIONS OF END



Type of Torispherical End: Dished End KORBOGEN DIN 28013-28014/SMS 482

WELD JOINT COEFFICIENT: Unwelded Component(z=1.0)

OUTSIDE DIAMETER OF CYLINDRICAL FLANGE OF END.....:De 324.00 mm

LENGTH OF CYLINDRICAL FLANGE OF END.....:Lcyl 20.00 mm

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....:th 0.3000 mm

NOMINAL THICKNESS OF HEAD/END (uncorroded).....:en 4.0000 mm

Include calculation of forming during fabrication to EN13445-4 Section 9.: NO

MATERIAL DATA FOR END

EN 10028-2:2017, 1.0473 P355GH plate and strip, HT:N THK<=16mm 130'C

Rm=510 Rp=355 Rpt=308.6 f=205.73 f20=212.5 ftest=338.1 E=203868(N/mm2) ro=7.85

Material & Delivery Form: NOT Cold Spun Seamless Austenitic Stainless Steel

NOZZLES IN KNUCKLE REGION TO SECTION 7.7

Nozzles In Knuckle Region: NO

WELDING REQUIREMENTS TO EN 1708-1:2010

Comment(Optional):

Type of welded connection: Not Applicable

CALCULATION DATA

7.5.3 - TORISPHERICAL ENDS UNDER INTERNAL PRESSURE

7.5.3.2 Required Minimum End Thickness

Required Thickness of End to Limit Membrane Stress in Central Part

$$e_s = P * R / (2 * f * z - 0.5 * P) \quad (7.5-1)$$

$$= 3.3 * 259.2 / (2 * 205.73 * 1 - 0.5 * 3.3) = 2.0872 \text{ mm}$$

$$f_b = R_{pt} / 1.5 \quad (7.5-4) = 308.6 / 1.5 = 205.73 \text{ N/mm}^2$$

Required Thickness of Knuckle to Avoid Plastic Buckling

$$e_b = (0.75 * R + 0.2 * D_i) * ((P / (111 * f_b)) * (D_i / r)^{0.825})^{(0.667)} \quad (7.5-3)$$

$$= (0.75 * 259.2 + 0.2 * 317) * ((3.3 / (111 * 205.73)) * (317 / 49.896)^{0.825})^{(0.667)}$$

$$= 1.9579 \text{ mm}$$

7.5.3.5 Formulas for Calculation of Factor Beta

$$Y = \text{MIN}(e_{min} / R, 0.04) \quad (7.5-9) = \text{MIN}(2.6201 / 259.2, 0.04) = 0.0101$$

$$Z = \text{LOG}(1 / Y) \quad (7.5-10) = \text{LOG}(1 / 0.0101) = 1.9953$$

$$X = r / D_i \quad (7.5-11) = 49.896 / 318.76 = 0.1565$$

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Botom Head 28 May 2023 11:42 ConnID:S1.1

$$N = 1.006 - 1 / (6.2 + (90 * Y) ^ 4) \quad (7.5-12)$$

$$= 1.006 - 1 / (6.2 + (90 * 0.0101) ^ 4) = 0.8608$$

$$\text{Beta01} = N * (-0.1833 * Z^3 + 1.0383 * Z^2 - 1.2943 * Z + 0.837) \quad (7.5-15)$$

$$= 0.8608 * (-0.1833 * 2.^3 + 1.0383 * 2.^2 - 1.2943 * 2. + 0.837) = 0.8023$$

$$\text{Beta02} = \text{MAX}(0.5, 0.95 * (0.56 - 1.94 * Y - 82.5 * Y ^ 2)) \quad (7.5-17)$$

$$= \text{MAX}(0.5, 0.95 * (0.56 - 1.94 * 0.0101 - 82.5 * 0.0101^2)) = 0.5054$$

$$\text{beta} = 10 * ((0.2 - X) * \text{Beta01} + (X - 0.1) * \text{Beta02}) \quad (7.5-16)$$

$$= 10 * ((0.2 - 0.1565) * 0.8023 + (0.1565 - 0.1) * 0.5054) = 0.6344$$

Required Thickness of Knuckle to Avoid Axisymmetric Yielding

$$e_y = \text{beta} * P * (0.75 * R + 0.2 * D_i) / f \quad (7.5-2)$$

$$= 0.6344 * 3.3 * (0.75 * 259.2 + 0.2 * 318.76) / 205.73 = 2.6272 \text{ mm}$$

NOTE 3, since $e_y(2.6) > 0.005 * D_i(1.6)$ it is NOT necessary to calculate/consider eb.

Required Minimum End Thickness Excl.Allow. e_{min} :

$$e_{min} = e_{min} = 2.63 = 2.6272 \text{ mm}$$

Required Minimum End Thickness Incl.Allow. :

$$e_{minA} = e_{min} + c + t_h = 2.63 + 0.5 + 0.3 = 3.4300 \text{ mm}$$

Internal Pressure $e_{minA}=3.43 \leq e_n=4$[mm]	85.7%	OK
--	--------------	-----------

Analysis Thickness

$$e_a = e_n - c - t_h = 4 - 0.5 - 0.3 = 3.2000 \text{ mm}$$

Inside Diameter of Shell

$$D_i = D_e - 2 * (e_n - c) = 324 - 2 * (4 - 0.5) = 317.00 \text{ mm}$$

Mean Diameter of Shell

$$D_m = (D_e + D_i) / 2 = (324 + 317) / 2 = 320.50 \text{ mm}$$

7.5.3.4 - Required Minimum Thickness of Straight Cylindrical Flange

$$L_{lim} = 0.2 * \text{SQRT}(D_i * e_{min}) = 0.2 * \text{SQRT}(317 * 2.63) = 5.7717 \text{ mm}$$

Since $L_{cyl} > L_{lim}$, Required Thickness of Straight Cylindrical Flange to 7.4.2

Minimum Thickness of Straight Flange Excl. Allow.

$$e_{cyl} = P * D_i / (2 * f * z - P) \quad (7.4-1)$$

$$= 3.3 * 317 / (2 * 205.73 * 1 - 3.3) = 2.5630 \text{ mm}$$

Minimum Thickness of Straight Flange Incl.Corr. :

$$e_{cylA} = e_{cyl} + c = 2.56 + 0.5 = 3.0600 \text{ mm}$$

7.5.3.1 Conditions of Applicability - Torispherical Ends

»Geometry Check $r=49.896 \leq 0.2 * D_i=63.4$ [mm] « » OK«

»Geometry Check $r=49.896 \geq 0.06 * D_i=19.02$ [mm] « » OK«

»Geometry Check $r=49.896 \geq 2 * e=5.25$ [mm] « » OK«

»Geometry Check $e=2.63 \leq 0.08 * D_e=25.92$ [mm] « » OK«

»Geometry Check $e_a=3.2 \geq 0.001 * D_e=0.324$ [mm] « » OK«

»Geometry Check $R=259.2 \leq D_e=324$ [mm] « » OK«

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :NEW & COLD

$$P_s = 2 * f * z * e_a / (R + 0.5 * e_a) \quad (7.5-6)$$

$$= 2 * 212.5 * 1 * 3.7 / (258.7 + 0.5 * 3.7) = 6.0353 \text{ MPa}$$

$$P_y = f * e_a / (\text{beta} * (0.75 * R + 0.2 * D_i)) \quad (7.5-7)$$

$$= 212.5 * 3.7 / (0.604 * (0.75 * 258.7 + 0.2 * 317)) = 5.0565 \text{ MPa}$$

$$P_b = 111 * f_b * (e_a / (0.75 * R + 0.2 * D_i)) ^ 1.5 * (r / D_i) ^ 0.825 \quad (7.5-8)$$

$$= 111 * 236.67 * (3.7 / (0.75 * 258.7 + 0.2 * 317)) ^ 1.5 * (49.896 / 317) ^ 0.825 = 9.8473 \text{ MPa}$$

$$P_{cyl} = 2 * e_a * f * z / (D_i + e_a)$$

$$= 2 * 3.7 * 212.5 * 1 / (317 + 3.7) = 4.9033 \text{ MPa}$$

P_{max} (is the least of P_s , P_y , P_b and P_{cyl}) = P_{max}

$$= 4.9 = 4.9033 \text{ MPa}$$

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :HOT & CORR

$$P_s = 2 * f * z * e_a / (R + 0.5 * e_a) \quad (7.5-6)$$

$$= 2 * 205.73 * 1 * 3.2 / (259.2 + 0.5 * 3.2) = 5.0486 \text{ MPa}$$

$$P_y = f * e_a / (\text{beta} * (0.75 * R + 0.2 * D_i)) \quad (7.5-7)$$

$$= 205.73 * 3.2 / (0.6135 * (0.75 * 259.2 + 0.2 * 317)) = 4.1622 \text{ MPa}$$

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Botom Head 28 May 2023 11:42 ConnID:S1.1

$$P_B = 111 * f_b * (e_a / (0.75 * R + 0.2 * D_i))^{1.5} * (r / D_i)^{0.825} \quad (7.5-8)$$
$$= 111 * 205.73 * (3.2 / (0.75 * 259.2 + 0.2 * 317))^{1.5} * (49.896 / 317)^{0.825} = 6.8700 \text{ MPa}$$
$$P_{cyl} = 2 * e_a * f * z / (D_i + e_a)$$
$$= 2 * 3.2 * 205.73 * 1 / (317 + 3.2) = 4.1120 \text{ MPa}$$
$$P_{max} \text{ (is the least of } P_s, P_y, P_b \text{ and } P_{cyl}) = P_{max}$$
$$= 4.11 = \underline{\underline{4.1120 \text{ MPa}}}$$

MAX TEST PRESSURE (Uncorroded cond.at ambient temp.)

$$P_s = 2 * f * z * e_a / (R + 0.5 * e_a) \quad (7.5-6)$$
$$= 2 * 338.1 * 1 * 3.7 / (258.7 + 0.5 * 3.7) = 9.6025 \text{ MPa}$$
$$P_y = f * e_a / (\beta * (0.75 * R + 0.2 * D_i)) \quad (7.5-7)$$
$$= 338.1 * 3.7 / (0.604 * (0.75 * 258.7 + 0.2 * 317)) = 8.0452 \text{ MPa}$$
$$P_B = 111 * f_b * (e_a / (0.75 * R + 0.2 * D_i))^{1.5} * (r / D_i)^{0.825} \quad (7.5-8)$$
$$= 111 * 338.1 * (3.7 / (0.75 * 258.7 + 0.2 * 317))^{1.5} * (49.896 / 317)^{0.825} = 14.07 \text{ MPa}$$
$$P_{cyl} = 2 * e_a * f * z / (D_i + e_a)$$
$$= 2 * 3.7 * 338.1 * 1 / (317 + 3.7) = 7.8015 \text{ MPa}$$
$$P_{max} \text{ (is the least of } P_s, P_y, P_b \text{ and } P_{cyl}) = P_{max}$$
$$= 7.8 = \underline{\underline{7.8015 \text{ MPa}}}$$

EN13445-5;10.2.3.3 REQUIRED MIN.HYDROSTATIC TEST PRESSURE:Ptmin

NEW AT AMBIENT TEMP. FOR TEST GROUPS 1, 2 and 3

$$P_{tmin} = 1.25 * P_d * f_{20} / f = 1.25 * 3.3 * 212.5 / 205.73 = \underline{\underline{4.2607 \text{ MPa}}}$$

$$P_{tmin} = 1.43 * P_d = 1.43 * 3.3 = \underline{\underline{4.7190 \text{ MPa}}}$$

Test Pressure Ptmin=4.72 <= Pmax=7.8[MPa]**60.4%****OK**

Maximum diameter of Opening Not Requiring Reinforcement Check , dmax

$$r_{is} = R \quad (9.5-4) = 259.2 = 259.20 \text{ mm}$$
$$\text{Length of Shell Contributing to Reinforcement}$$
$$I_s = \text{Sqr}((2 * r_{is} + e_a) * e_a) \quad (9.5-2)$$
$$= \text{Sqr}((2 * 259.2 + 3.2) * 3.2) = 40.85 \text{ mm}$$
$$\text{Maximum Diameter of Unreinforced Opening in Shell Checked to Rules in Section 9}$$
$$d_{max1} = \text{MIN}(0.5 * D_i, (e_a * I_s * (f - 0.5 * P) / P - r_{is} * I_s) / (0.5 * r_{is} + 0.5 * e_a)) \quad (9.5-7, 22, 23)$$
$$= \text{MIN}(0.5 * 317, (3.2 * 40.85 * (205.73 - 0.5 * 3.3) / 3.3 - 259.2 * 40.85) / (0.5 * 259.2 + 0.5 * 3.2)) = \underline{\underline{0.00 \text{ mm}}}$$
$$\text{Maximum diameter of Opening Not Requiring Reinforcement Check}$$
$$d_{max2} = 0.15 * \text{Sqr}((2 * r_{is} + e_a) * e_a) \quad (9.5-18)$$
$$= 0.15 * \text{Sqr}((2 * 259.2 + 3.2) * 3.2) = \underline{\underline{6.1282 \text{ mm}}}$$
$$\text{Maximum Diameter of Unreinforced Opening}$$
$$d_{max} = \text{MAX}(d_{max1}, d_{max2}) = \text{MAX}(0, 6.13) = \underline{\underline{6.1282 \text{ mm}}}$$

CALCULATION SUMMARY

7.5.3 - TORISPHERICAL ENDS UNDER INTERNAL PRESSURE

7.5.3.2 Required Minimum End Thickness

$$\text{Required Minimum End Thickness Excl.Allow. } e_{min} :$$
$$e_{min} = e_{min} = 2.63 = \underline{\underline{2.6272 \text{ mm}}}$$

$$\text{Required Minimum End Thickness Incl.Allow. } :$$
$$e_{min_a} = e_{min} + c + t_h = 2.63 + 0.5 + 0.3 = \underline{\underline{3.4300 \text{ mm}}}$$

Internal Pressure emina=3.43 <= en=4[mm]**85.7%****OK**

Minimum Thickness of Straight Flange Incl.Corr. :

$$e_{cyl_a} = e_{cyl} + c = 2.56 + 0.5 = \underline{\underline{3.0600 \text{ mm}}}$$

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :NEW & COLD

$$P_{max} \text{ (is the least of } P_s, P_y, P_b \text{ and } P_{cyl}) = P_{max}$$
$$= 4.9 = \underline{\underline{4.9033 \text{ MPa}}}$$

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Botom Head 28 May 2023 11:42 ConnID:S1.1

MAXIMUM ALLOWABLE WORKING PRESSURE MAWP :HOT & CORRPmax (is the least of Ps, Py, Pb and Pcyl) = Pmax
=4.11=

4.1120 MPa

MAX TEST PRESSURE (Uncorroded cond.at ambient temp.)Pmax (is the least of Ps, Py, Pb and Pcyl) = Pmax
=7.8=

7.8015 MPa

EN13445-5;10.2.3.3 REQUIRED MIN.HYDROSTATIC TEST PRESSURE:Ptmin

NEW AT AMBIENT TEMP. FOR TEST GROUPS 1, 2 and 3

Ptmin = 1.25 * Pd * f20 / f =1.25*3.3*212.5/205.73=

4.2607 MPa

Ptmin = 1.43 * Pd =1.43*3.3=

4.7190 MPa

Test Pressure Ptmin=4.72 <= Pmax=7.8[MPa]**60.4%****OK****Maximum diameter of Opening Not Requiring Reinforcement Check , dmax**

Maximum Diameter of Unreinforced Opening

dmax = MAX(dmax1, dmax2) =MAX(0,6.13)=

6.1282 mm

Volume:0.0058 m3 Weight:4.2 kg (SG= 7.85)

Company Name -

Client :GÜVEN SOGUTMA

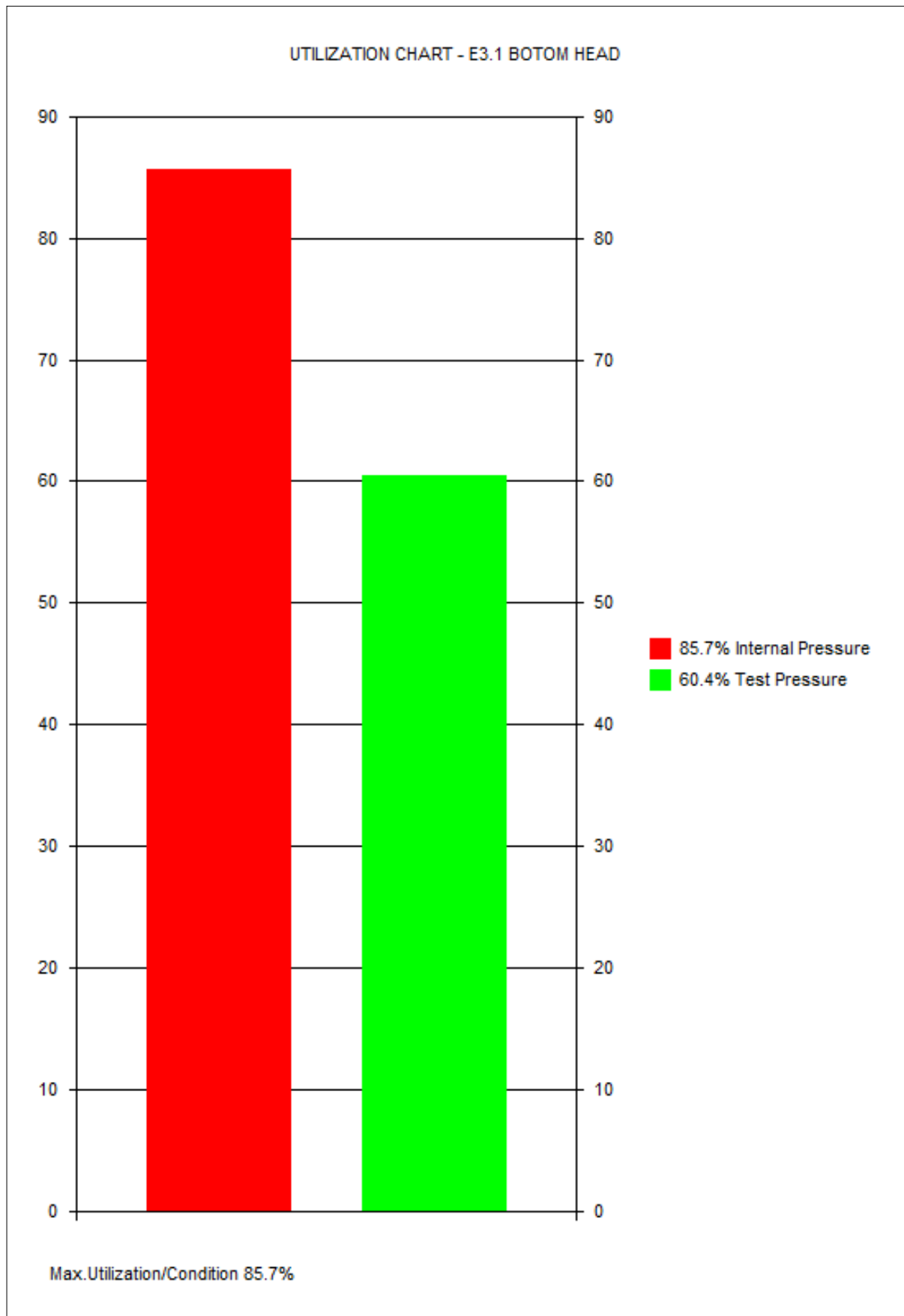
Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 7.5 DOMED ENDS

E3.1 Botom Head

28 May 2023 11:42 ConnID:S1.1



Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.1 ROT 1 3/4"

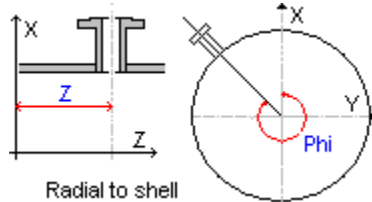
28 May 2023 11:46 ConnID:S1.1

INPUT DATA

COMPONENT ATTACHMENT/LOCATION

Attachment: S1.1 Cylindrical Shell Main Shell

Connect this nozzle to the nozzle neck of another nozzle: NO

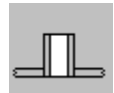


Orientation & Location of Nozzle: Radial to Shell

z-location of nozzle along axis of attachment.....:z 480.00 mm

Angle of Rotation of nozzle axis projected in the x-y plane:Phi 180.00 Degr.

GENERAL DESIGN DATA



Type of Opening: Nozzle Without Standard ASME or DIN/EN Flange Attachment

PRESSURE LOADING: Design Component for Internal Pressure Only

PROCESS CARD:

General Design Data : Temp= 130°C, P=3.3000 MPa, c=0.5 mm, Pext=0.0000 MPa

SPECIFIC DENSITY OF OPERATING LIQUID.....:SG 0.00

LIQUID HEAD.....:LH 0.00 mm

Apply a different corrosion allowance to nozzle neck than the shell thickness.: NO

Include Nozzle Load Calculation: NO

SHELL DATA (S1.1)

Shell Type: Cylindrical Shell

OUTSIDE DIAMETER OF SHELL.....:De 324.00 mm

NOMINAL WALL THICKNESS (uncorroded).....:en 4.0000 mm

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....:th 0.3000 mm

EN 10217-3:2019, 1.0565 P355NH welded tube, HT:N THK<=20mm 130'C

Rm=490 Rp=355 Rpt=292 fs=194.67 f20=204.17 ftest=338.1 E=203868(N/mm2) ro=7.85

NOZZLE MATERIAL DATA



Delivery Form: Seamless Pipe

EN 10216-2:2013, 1.0345 P235GH seamless tube, HT:N THK<=16mm 130'C

Rm=360 Rp=235 Rpt=191.4 fb=127.6 f20=150 ftest=223.81 E=203868(N/mm2) ro=7.85

NOZZLE DIMENSIONAL DATA

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.1 ROT 1 3/4"

28 May 2023 11:46 ConnID:S1.1



Attachment: Set In Flush Nozzle

Shape of Nozzle/Opening: Circular

Application:

9.4.6.3 NOT a critical fatigue area, and calc.temp.is outside creep range.

OUTSIDE NOZZLE DIAMETER.....:deb 44.50 mm

NOMINAL NOZZLE THICKNESS (uncorroded).....:enb 8.4000 mm

Size of Flange and Nozzle:

Comment (Optional):

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....: 12.50 %

NOZZLE STANDOUT MEASURED FROM VESSEL OD.....:ho 40.00 mm

WELDING DATA

Nozzle/Pad to Shell Welding Area: Exclude Area of Nozzle to Shell Weld

Nozzle Weld Intersect: Nozzle Does NOT Intersect with a Welded Shell Seam

ANGLE PhiC(OBLIQUE IN TRANSVERSE.CROSS SECT.)Fig.9.5-2:PhiC 0.00 Degr.

ANGLE PhiL(OBLIQUE IN LONG.CROSS SECT.)Fig.9.5-1.....:PhiL 0.00 Degr.

DATA FOR REINFORCEMENT PAD



Type of Pad: No Pad

LIMITS OF REINFORCEMENT

Reduction of Limits of Reinforcement: No Reduction Required

WELDING REQUIREMENTS TO EN 1708-1:2010

Comment(Optional):

Type of welded connection: Not Applicable

CALCULATION DATA

PRELIMINARY CALCULATIONS

Shell Analysis Thickness eas 3.2000 mm

eas = en - c - th =4-0.5-0.3=

Nozzle Analysis Thickness eab 6.8500 mm

eab = enb - cn - NegDev =8.4-0.5-1.05=

Inside Radius of Curvature 158.80 mm

ris = De / 2 - eas (9.5-3) =324/2-3.2=

dib = deb - 2 * eab =44.5-2*6.85= 30.80 mm

Min.Nozzle Thk.Based on Internal Pressure ebp

ebp = P * deb / (2 * fb * z + P) 0.5700 mm

=3.3*44.5/(2*127.6*1+3.3)=

Allowable Stresses 127.60 N/mm2

fob = Min(fs, fb) (9.5-8) =Min(194.67,127.6)=

GEOMETRIC LIMITATIONS

»Check Max.Diameter of Nozzle dib/(2*ris)=0.097 <= 1.00=1[mm] «» OK«

Min.Nozzle Thk. ebp=0.57 <= eab=6.85[mm]	8.3%	OK
--	------	----

9.5.2.4.4 Nozzles normal to the shell, with or without reinforcement pads.

Calculation of Stress Loaded Areas Effective as Reinforcement

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.1 ROT 1 3/4" 28 May 2023 11:46 ConnID:S1.1

Area of Shell Afs

Limit of Reinforcement Along Shell

Iso = Sqr((2 * ris + eas) * eas)

=Sqr((2*158.8+3.2)*3.2)=

32.04 mm

Set In Nozzle

Afs = eas * Is (9.5-79) =3.2*32.04=

102.53 mm2

Area of Nozzle Afb

Limit of Reinforcement Along Nozzle (outside shell)

Ibo = MIN(Sqr((deb - eb) * eb), ho)

(9.5-76)

=MIN(Sqr((44.5-6.85)*6.85),40)=

16.06 mm

Set In Nozzle

Afb = eb * (Ibo + Ibi + eas) (9.5-78) =6.85*(16.06+0+3.2)=

131.93 mm2

Calculation of Pressure Loaded Areas

In the Nozzle Apb

Apb = 0.5 * dib * (Ibo + eas) (9.5-84) =0.5*30.8*(16.06+3.2)=

296.59 mm2

Cyl.Shell in the Longitudinal Section ApsL

ApsL = ris * (Is + a) (9.5-94) =158.8*(32.04+22.25)=

8621.25 mm2

Cyl.Shell in the Transverse Cross Section ApsT

ApsT = 0.5 * ris ^ 2 * (Is + a) / (0.5 * eas + ris)

(9.5-105)

=0.5*158.8^2*(32.04+22.32)/(0.5*3.2+158.8)=

4273.28 mm2

Aps = MAX(ApsL ApsT) =MAX(8621.25,4273.28)=

8621.25 mm2

9.5.2 Reinforcement Rules

Pressure Area Required pA(req.)

pAREqL = P * (ApsL + Apb + 0.5 * ApphiL)

(9.5-7)

=3.3*(8621.25+296.59+0.5*0)=

29.43 kN

pAREqT = P * (ApsT + Apb + 0.5 * Apphi)

(9.5-7)

=3.3*(4273.28+296.59+0.5*0)=

15.08 kN

pAREq = MAX(pAREqL, pAREqT) =MAX(29428.88,15080.6)=

29.43 kN

Pressure Area Available pA(aval.)

pAAval = (Afs+Afw)*(fs-0.5*P)+Afp*(fop-0.5*P)+Afb*(fob-0.5*P)

(9.5-7)

=(102.53+0)*(194.67-0.5*3.3)+0*(0-0.5*3.3)+131.93*(127.6-0.5*3.3)=

36.41 kN

Nozzle Reinforcement pAAval=36.41 >= pAREq=29.43[kN]

80.8%

OK

Maximum Allowable Pressure Pmax

Pmax = (Afs+Afw)*fs+Afb*fob/((ApsL+Apb)+0.5*(Afs+Afw+Afb+Afp))

(9.5-10)

=(102.53+0)*194.67+131.93*127.6/((8621.25+296.59)+0.5*(102.53+0+131.93+0))

= 4.0722 MPa

Max.Allowable Test Pressure Pmax

Ptmax = ==

7.9314 MPa

Weight of Nozzle: .3408kg

CALCULATION SUMMARY

Min.Nozzle Thk. ebp=0.57 <= eab=6.85[mm]

8.3%

OK

9.5.2.4.4 Nozzles normal to the shell, with or without reinforcement pads.

Limit of Reinforcement Along Shell

Iso = Sqr((2 * ris + eas) * eas)

=Sqr((2*158.8+3.2)*3.2)=

32.04 mm

Limit of Reinforcement Along Nozzle (outside shell)

Ibo = MIN(Sqr((deb - eb) * eb), ho)

(9.5-76)

7 N.1 Nozzle,Seamless Pipe ROT 1 3/4"

Umax= 80.8%

Page: 13

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.1 ROT 1 3/4" 28 May 2023 11:46 ConnID:S1.1

$$=\text{MIN}(\text{Sqr}((44.5-6.85)*6.85),40)=$$

16.06 mm

Pressure Area Required pA(req.)

$$pAReqL = P * (ApsL + Apb + 0.5 * ApphiL)$$

(9.5-7)

$$=3.3*(8621.25+296.59+0.5*0)=$$

29.43 kN

$$pAReqT = P * (ApsT + Apb + 0.5 * Apphi)$$

(9.5-7)

$$=3.3*(4273.28+296.59+0.5*0)=$$

15.08 kN

$$pAReq = \text{MAX}(pAReqL, pAReqT) = \text{MAX}(29428.88, 15080.6) =$$

29.43 kN

Pressure Area Available pA(aval.)

$$pAAval = (Afs+Afw)*(fs-0.5*P)+Afp*(fop-0.5*P)+Afb*(fob-0.5*P)$$

(9.5-7)

$$=(102.53+0)*(194.67-0.5*3.3)+0*(0-0.5*3.3)+131.93*(127.6-0.5*3.3)=$$

36.41 kN

Nozzle Reinforcement pAAval=36.41 >= pAReq=29.43[kN]**80.8%****OK****Maximum Allowable Pressure Pmax**

$$Pmax = (Afs+Afw)*fs+Afb*fob/((ApsL+Apb)+0.5*(Afs+Afw+Afb+Afp))$$

(9.5-10)

$$=(102.53+0)*194.67+131.93*127.6/((8621.25+296.59)+0.5*(102.53+0+131.93+0))$$

$$= 4.0722 \text{ MPa}$$

Volume:0.00 m3 Weight:0.3 kg (SG= 7.85)

Company Name -

Client :GÜVEN SOGUTMA

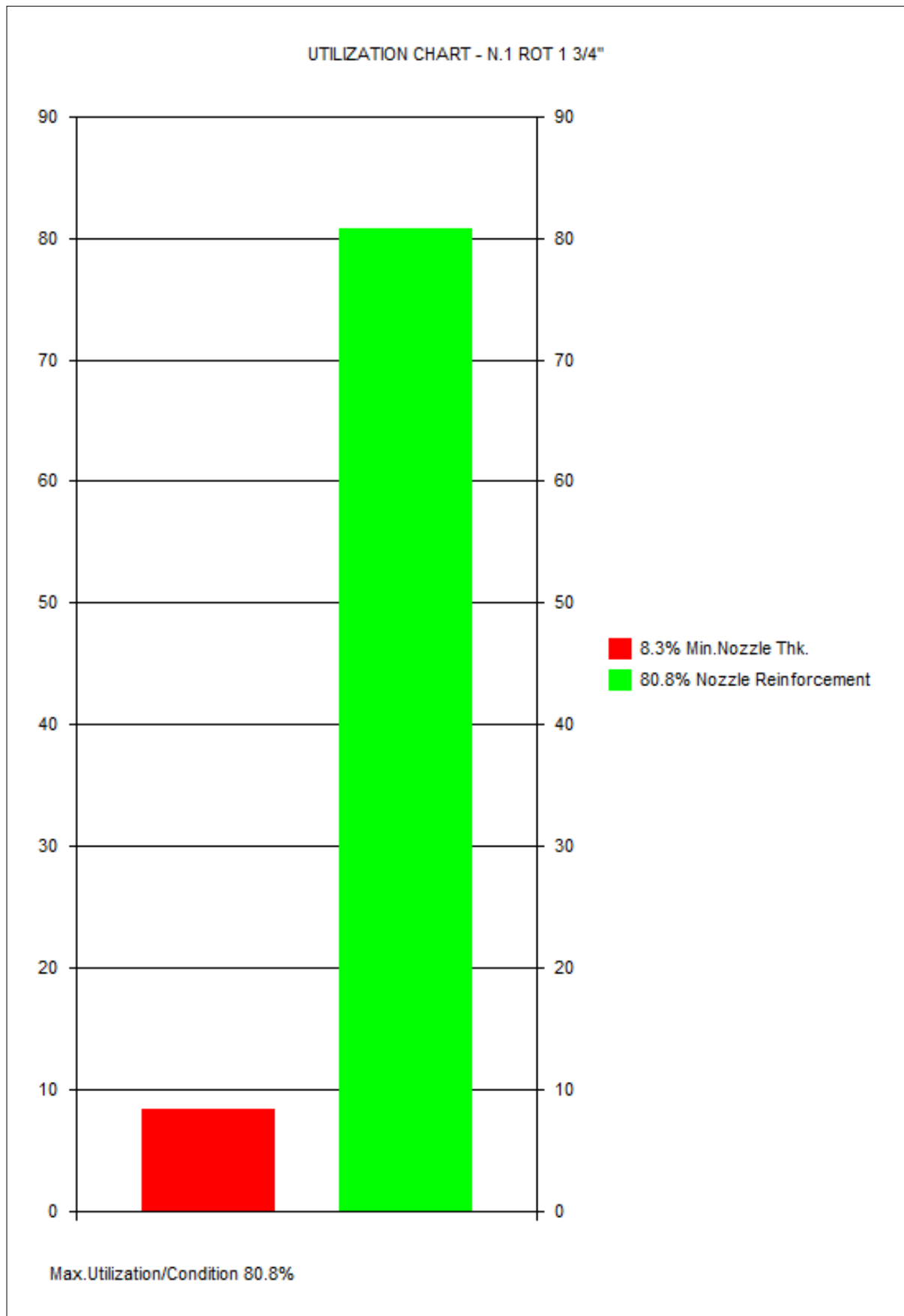
Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.1 ROT 1 3/4"

28 May 2023 11:46 ConnID:S1.1



Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.3 1/2" NPT

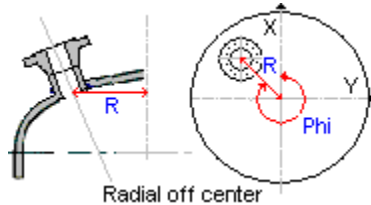
28 May 2023 11:46 ConnID:E3.2*

INPUT DATA

COMPONENT ATTACHMENT/LOCATION

Attachment: E3.2* Torispherical End Upper Head Sl.1

Connect this nozzle to the nozzle neck of another nozzle: NO

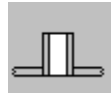


Orientation & Location of Nozzle: Radial to End (Off Center)

Angle of Rotation of nozzle axis projected in the x-y plane:Phi 180.00 Degr.

Distance between Center of End and Center of Nozzle.:R 100.00 mm

GENERAL DESIGN DATA



Type of Opening: Nozzle Without Standard ASME or DIN/EN Flange Attachment

PRESSURE LOADING: Design Component for Internal Pressure Only

PROCESS CARD:

General Design Data : Temp= 130°C, P=3.3000 MPa, c=0.5 mm, Pext=0.0000 MPa

SPECIFIC DENSITY OF OPERATING LIQUID.....:SG 0.00

LIQUID HEAD.....:LH 0.00 mm

Apply a different corrosion allowance to nozzle neck than the shell thickness.: NO

Include Nozzle Load Calculation: NO

SHELL DATA (E3.2*)

Shell Type: Torispherical End

OUTSIDE DIAMETER OF SHELL.....:De 324.00 mm

NOMINAL WALL THICKNESS (uncorroded).....:en 4.0000 mm

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....:th 0.3000 mm

INSIDE SPHERICAL RADIUS (corroded).....:R 259.20 mm

EN 10028-2:2017, 1.0473 P355GH plate and strip, HT:N THK<=16mm 130'C

Rm=510 Rp=355 Rpt=308.6 fs=205.73 f20=212.5 ftest=338.1 E=203868(N/mm2) ro=7.85

NOZZLE MATERIAL DATA



Delivery Form: Seamless Pipe

EN 10216-2:2013, 1.0345 P235GH seamless tube, HT:N THK<=16mm 130'C

Rm=360 Rp=235 Rpt=191.4 fb=127.6 f20=150 ftest=223.81 E=203868(N/mm2) ro=7.85

NOZZLE DIMENSIONAL DATA

Company Name -

Client :GÜVEN SOGUTMA

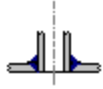
Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.3 1/2" NPT

28 May 2023 11:46 ConnID:E3.2*



Attachment: Set In Flush Nozzle

Shape of Nozzle/Opening: Circular

Application:

9.4.6.3 NOT a critical fatigue area, and calc.temp.is outside creep range.

OUTSIDE NOZZLE DIAMETER.....:deb 31.50 mm

NOMINAL NOZZLE THICKNESS (uncorroded).....:enb 7.0500 mm

Size of Flange and Nozzle:

Comment (Optional):

NEGATIVE TOLERANCE/THINNING ALLOWANCE.....: 12.50 %

NOZZLE STANDOUT MEASURED FROM VESSEL OD.....:ho 30.00 mm

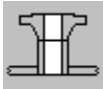
WELDING DATA

Nozzle/Pad to Shell Welding Area: Exclude Area of Nozzle to Shell Weld

Nozzle Weld Intersect: Nozzle Does NOT Intersect with a Welded Shell Seam

ANGLE BETWN.BRANCH AXIS AND A LINE NORMAL TO MAIN BODY:Phi 0.00 Degr.

DATA FOR REINFORCEMENT PAD



Type of Pad: No Pad

LIMITS OF REINFORCEMENT

Reduction of Limits of Reinforcement: No Reduction Required

WELDING REQUIREMENTS TO EN 1708-1:2010

Comment(Optional):

Type of welded connection: Not Applicable

CALCULATION DATA

PRELIMINARY CALCULATIONS

Shell Analysis Thickness eas
eas = en - c - th =4-0.5-0.3= 3.2000 mm

Nozzle Analysis Thickness eab
eab = enb - cn - NegDev =7.05-0.5-0.8813= 5.6688 mm

ris = R (9.5-4) =100= 259.20 mm

dib = deb - 2 * eab =31.5-2*5.67= 20.16 mm

Min.Nozzle Thk.Based on Internal Pressure ebp

ebp = P * deb / (2 * fb * z + P)
=3.3*31.5/(2*127.6*1+3.3)= 0.4000 mm

Allowable Stresses

fob = Min(fs, fb) (9.5-8) =Min(205.73,127.6)= 127.60 N/mm²

GEOMETRIC LIMITATIONS

»Check Max.Diameter of Nozzle dib/De=0.0622 <= 0.60=0.6[mm] (9.4.5.3)«» OK«

Min.Nozzle Thk. ebp=0.4 <= eab=5.67[mm]	7.0%	OK
---	------	----

»Location in End to Fig.9.5-4 L=47.02 >= De/10=32.4[mm] « » OK«

9.5.2.4.4 Nozzles normal to the shell, with or without reinforcement pads.

Calculation of Stress Loaded Areas Effective as Reinforcement

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.3 1/2" NPT

28 May 2023 11:46 ConnID:E3.2*

Area of Shell Afs

Limit of Reinforcement Along Shell Reduced by Location in Dished End

Iso = == 17.04 mm

Set In Nozzle

Afs = eas * Is (9.5-79) = 3.2*17.04= 54.53 mm2

Area of Nozzle Afb

Limit of Reinforcement Along Nozzle (outside shell)

Ibo = MIN(Sqr((deb - eb) * eb), ho) (9.5-76)

=MIN(Sqr((31.5-5.67)*5.67),30)= 12.10 mm

Set In Nozzle

Afb = eb * (Ibo + Ibi + eas) (9.5-78) = 5.67*(12.1+0+3.2)= 86.74 mm2

Calculation of Pressure Loaded Areas

In the Nozzle Apb

Apb = 0.5 * dib * (Ibo + eas) (9.5-84) = 0.5*20.16*(12.1+3.2)= 154.25 mm2

Spherical Shell/End on any Section Aps

Aps = 0.5 * ris ^ 2 * (Is + a) / (0.5 * eas + ris) (9.5-105)

= 0.5*259.2^2*(17.04+15.76)/(0.5*3.2+259.2)= 4224.84 mm2

9.5.2 Reinforcement Rules

Pressure Area Required pA(req.)

pAReq = P * (Aps + Apb + 0.5 * Apphi) (9.5-7)

= 3.3*(4224.84+154.25+0.5*0)= 14.45 kN

Pressure Area Available pA(aval.)

pAAval = (Afs+Afw)*fs+Afb*fob/((Aps+Apb+0.5*Apphi)+0.5*(Afs+Afw+Afb+Afp)) (9.5-7)

= (54.53+0)*(205.73-0.5*3.3)+0*(0-0.5*3.3)+86.74*(127.6-0.5*3.3)= 22.05 kN

Nozzle Reinforcement pAAval=22.05 >= pAReq=14.45[kN]

65.5%

OK

Maximum Allowable Pressure Pmax

Pmax = (Afs+Afw)*fs+Afb*fob/((Aps+Apb+0.5*Apphi)+0.5*(Afs+Afw+Afb+Afp)) (9.5-10)

= (54.53+0)*205.73+86.74*127.6/((4224.84+154.25+0.5*0)+0.5*(54.53+0+86.74+0))= 5.0084 MPa

Max.Allowable Test Pressure P_{tmax}

P_{tmax} = == 9.5209 MPa

Weight of Nozzle: .1466kg

CALCULATION SUMMARY

Min.Nozzle Thk. ebp=0.4 <= eab=5.67[mm]

7.0%

OK

9.5.2.4.4 Nozzles normal to the shell, with or without reinforcement pads.

Limit of Reinforcement Along Shell Reduced by Location in Dished End

Iso = == 17.04 mm

Limit of Reinforcement Along Nozzle (outside shell)

Ibo = MIN(Sqr((deb - eb) * eb), ho) (9.5-76)

=MIN(Sqr((31.5-5.67)*5.67),30)= 12.10 mm

Pressure Area Required pA(req.)

pAReq = P * (Aps + Apb + 0.5 * Apphi) (9.5-7)

= 3.3*(4224.84+154.25+0.5*0)= 14.45 kN

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.3 1/2" NPT

28 May 2023 11:46 ConnID:E3.2*

Pressure Area Available pA(aval.)

$$pAAval = (Afs+Af_w) * (fs-0.5*P) + Afp * (fop-0.5*P) + Afb * (fob-0.5*P) \quad (9.5-7)$$

$$= (54.53+0) * (205.73-0.5*3.3) + 0 * (0-0.5*3.3) + 86.74 * (127.6-0.5*3.3) = \underline{\underline{22.05 \text{ kN}}}$$

Nozzle Reinforcement pAAval=22.05 >= pAReq=14.45[kN]**65.5%****OK****Maximum Allowable Pressure Pmax**

$$Pmax = (Afs+Af_w) * fs + Afb * fob / ((Aps+Apb+0.5*Apphi) + 0.5 * (Afs+Af_w+Af_b+Af_p)) \quad (9.5-10)$$

$$= (54.53+0) * 205.73 + 86.74 * 127.6 / ((4224.84+154.25+0.5*0) + 0.5 * (54.53+0+86.74+0)) = \underline{\underline{5.0084 \text{ MPa}}}$$

Volume:0.00 m3 Weight:0.1 kg (SG= 7.85)

Company Name -

Client :GÜVEN SOGUTMA

Vessel Tag No.:HV9.33b.60.A4.A4.F4

Visual Vessel Design by Hexagon PPM,Ver:20.0 Operator : Rev.:A

EN13445:2014 Issue 5+A8:2019 - 9.5 ISOLATED OPENINGS IN SHELLS

N.3 1/2" NPT

28 May 2023 11:46 ConnID:E3.2*

